

Faculty of Mechanical Engineering



Master of Science in Mechanical Engineering

INVESTIGATION OF OSCILLATORY-FLOW BEHAVIOUR ACROSS INTERNAL STRUCTURE IN THERMOACOUSTIC REFRIGERATION SYSTEM

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DECLARATION

I declare that this thesis entitled "Investigation of Oscillatory-Flow Behaviour Across Internal Structure in Thermoacoustic Refrigeration System" is the result of my own research except as cited in the references. The thesis has not been accepted for any degree and is not concurrently submitted in candidature of any other degree.



APPROVAL

I hereby declare that I have read this thesis and in my opinion this thesis is sufficient in terms of scope and quality for the award of Master of Science in Mechanical Engineering.



DEDICATION

In honour of my loving parents and siblings



ABSTRACT

Thermoacoustic technology has been recognised as the one of green technology as it provides alternatives green working mechanism for engine and refrigeration system. This is due to its simplicity (as there was no moving parts) and the system also use a non-polluting gas. Unfortunately, the fluid dynamics of the system is complex and not well understood. The fluid that flows inside the system is flowing in oscillatory conditions following the acoustic wave. In this study, flow distribution inside a standing wave thermoacoustic condition is tested experimentally and numerically. The thermoacoustic system is first modelled using DeltaE software. The model is used as benchmark for setting up of a thermoacoustic rig that is suitable for the investigation of the oscillatory flow behaviour across the internal structures in the thermoacoustic system. The components of the rig include the loudspeaker as the acoustic driver, a resonator made of steel and a structure known as a stack made of aluminium. The stack was a parallel-plate structure where most thermoacoustic effects take place. The test rig was build based on a quarter wavelength standing-wave thermoacoustic design. Therefore, for the purpose of investigating the fluid dynamics of oscillatory flow at different frequencies, the resonator was divided into several segments which was assembled according to flow frequency. Due to the complication of design, the study of flow frequencies was limited to only two flow frequencies, which were 14.2 Hz and 23.6 Hz. For 14.2 Hz flow frequencies, the stack was located at two different locations of 0.11λ and 0.18λ from the pressure antinode while 23.6 Hz flow frequencies, the stack was located at 0.18λ from the pressure antinode. The stack was fabricated with two different lengths of 70 mm and 200 mm. The experimental rig was first tested for resonance frequency and references point followed by the investigation of the change of velocity in each point along the thermoacoustic rig as drive ratio (ratio of pressure at antinode to the mean pressure) changes. The DeltaE software models provide pressure distribution data that are similar to the theoretical data and stack with the length of 200 mm gives a better performance in term of drive ratio (Dr) where an increment of drive ratio percentage of 28% was recorded compared to 25% drive ratio increment for the 70 mm stack. Comparisons were also made for first-order harmonic velocity amplitude, u_1 , obtained from three different methods; theoretical calculations, DeltaE software, and the experimentally measured values. It is found that the velocity distribution of flow across the 70 mm long stack results in highest Stoke's Reynolds number which is 271.99 that leads to early starts of turbulence in the flow. The stack's location of 0.11λ was also found to be the best location based on velocity data of the current flow conditions. Besides that, it is also found that 23.6 Hz flow frequency result in the better drive ratio compared to 14.2 Hz. The findings help to understand possible differences between theoretical and real experimental values so that better improvements can be made in the future design of the thermoacoustic system.

ABSTRAK

Sistem termoakustik telah diiktiraf sebagai sistem teknologi hijau yang menyediakan alternatif mekanisma kerja untuk enjin dan sistem penyejukan. Ini kerana keringkasannya (tiada bahagian bergerak) dan menggunakan gas bukan pencemar. Malangnya, sistem dinamik bendalir adalah kompleks dan masih belum difahami dengan baik. Cecair yang mengalir di dalam sistem ini adalah dalam keadaan berayun mengikut gelombang akustik. Dalam penyiasatan ini, pengagihan aliran dalam keadaan gelombang termoakustik berdiri diuji secara ekserimen dan berangka. Sistem termoakustik ini dimodelkan menggunakan perisian DeltaE. Model ini digunakan sebagai penanda aras untuk membina rig eksperimen thermoakustik yang sesuai dalam menyiasat kelakuan aliran berayun disepanjang struktur dalam sistem termoakustik. Komponennya adalah pembesar suara sebagai pemacu akustik, sebuah 'resonator' yang diperbuat daripada keluli dan satu struktur yang dikenali sebagai timbunan yang diperbuat daripada aluminium. Timbunan ini adalah struktur plat selari di mana kebanyakan kesan-kesan termoakustik berlaku. Rig ini dibina mengikut reka bentuk suku gelombang termoakustik berdiri. Maka, untuk menyiasat sistem dinamik bendalir aliran berayun, 'resonator' telah dibahagikan kepada beberapa segmen yang disusun mengikut kepanjangan frekuensi aliran. Disebabkan komplikasi reka bentuk, penyiasatan frekuensi aliran hanya terhad kepada dua frekuensi aliran iaitu 14.2 Hz dan 23.6 Hz. Bagi 14.2 Hz frekuensi aliran, timbunan telah diletakkan di dua bahagia berlainan iaitu 0.11λ dan 0.18^{\lambda} dari antinod tekanan manakala bagi 23.6 Hz frekuensi aliran, timbunan diletakkan pada 0.18 λ dari antinod tekanan. Timbunan dibina dengan dua kepanjangan berbeza iaitu 70 mm dan 200 mm. Rig eksperimen awalnya diuji dengan frekuensi resonan dan titik rujukan diikuti penyiasatan perubahan halaju di setiap titik di sepanjang rig termoakustik sebagai nisbah pemacu (nisbah tekanan pada antinod kepada tekanan purata). Model perisian DeltaE mengeluarkan data tekanan pengedaran yang serupa dengan data teori dan timbunan dengan kepanjangan 200 mm memberikan prestasi lebih baik dengan kenaikan 28% nisbah tekanan berbanding timbunan panjang 70 mm yang hanya mencatatkan kenaikan 25% nisbah tekanan. Perbandingan dari segi amplitud halaju harmonic pertama, u₁, telah diperoleh dari tiga kaedah berbeza iaitu pengiraan teori, perisian DeltaE dan ekperimen. Halaju pengagihan aliran melalui timbunan 70 mm telah dikenalpasti menghasilkan nombor 'Stoke's Reynolds' yang lebih tinggi dan juga membawa kepada pergolakan awal dalam aliran. Lokasi timbunan pada 0.17λ dari antinod tekanan juga dikenalpasti merupakan lokasi terbaik berdasarkan data halaju pada aliran semasa. Selain itu, aliran frekuensi 23.6 Hz didapati mempunyai nisbah pemacu yang lebih baik berbanding 14.2 Hz. Dapatan kajian ini membantu dalam memahami kemungkinan perbezaan antara nilai teori dan eksperimen bagi penambahbaikan reka bentuk sistem termoakustik akan datang.

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LIST OF SYMBOLS

a	-	Speed of sound
С	-	Specific heat capacity
С	-	Speed of light
c_p	-	Isobaric specific heat per unit mass
Dr	-	Drive ratio
f	-	Frequency
K	-	Thermal conductivity
l	-	Length
М	-	Metre
mm	-	Millimetre
P_m	-	Mean pressure
P_a	-	Pressure at antinode
R	-	Gas constant
Re	-	Reynolds number
Т	- 6	Temperature
u_1	-	First order harmonic velocity amplitude
V	-	Volts
Ŵ	-	Acoustic work
X_S	-	Distance between the pressure antinode of the resonator to the centre of the
		stack
x_o	-	Centre of the stack
Уo	-	Half of plate spacing
γ	-	Ratio of specific heat capacities
λ	-	Wavelength
ω	-	Angular velocity
δ	-	Ratio of velocity amplitude and angular frequency
ξ	-	Gas displacement
δ_k	-	Thermal penetration depth
δ_v	-	Viscous penetration depth
κ	-	The diffusivity of the gas
ho	-	Mean density of the gas
μ	-	Dynamic viscosities
v	-	kinematic viscosities
σ	-	Prandtl number
ø	-	Porosity
γ_h	-	Hydraulic radius
ϵ_{s}	-	Heat capacity ratio

LIST OF PUBLICATIONS

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Johari, D., Mat Tokit, E., and Mohd Saat, F.A.Z. 2016. *Instrumentation for Studying the Turbulence Characteristic in Oscillatory Flow Used in Thermoacoustic: A Review.* Postgraduates Symposium for Environment Engineering Technology.

CHAPTER 1

INTRODUCTION

1.1 Research background

Generally, thermoacoustic technology is based on the system of 'thermoacoustic effect' and can be divided into two systems, which are refrigerator and heat engine. It is a system that uses acoustic energy and thermal energy conversion without any moving parts in the system, which using non-polluting gases such as helium, argon, xenon, or also known as inert gases. The thermoacoustic technology encompasses the fields of thermodynamics and acoustics as it consumes a little energy input besides the minimum range of fabrication cost. This technology has been very compromising in developing green technology that is advancing rapidly day by day.

Nowadays, green technologies are being developed continuously around the world as the greenhouse effects and climate change is very alarming. This is due to the usage of chemicals that is increasing uncontrollably, such as Chlorofluorocarbon (CFC) that is being used in the cooling system. Scientists and researchers all around the globe are intensely finding new technology and innovation to solve this problem. However, green technologies come with some significant issues such as a very high cost to comply with the existing technology.

Chlorofluorocarbon (CFC) is a stable compound that had been the most common chemical used in many applications such as refrigerant, solvent, synthesis of the plastic and also for many other applications. Even though it has been used in many forms, it is a compound that is non-flammable, tasteless, odorless and not easily being decomposed which causes a negative effect on the environment and depletion of the ozone layer due to its physical characteristic and heat resistance. Due to this effect, it has been banned from some of the countries to protect the environment. As the effect of the prohibited of the CFC, many researchers give a particular interest in developing green technology to replace the current use of CFC. Thermoacoustic refrigerator and engine are one of the alternatives that have been developed with no refrigerant at all but still in the early investigation due to the unclear effects and its performances.

Back in the 19th century, Rayleigh started the theoretical basis of the acoustic field. In the thermoacoustic system, the exchanging of gas-particle from cold to the hot reservoir was set at the place where there is a supply of acoustic energy at the region of a solid boundary by using a stack, which is in the form of porous shape or parallel plates. The expansion and contraction of the gas particles together with their oscillatory movement allow energy transport and creates a temperature gradient. At an optimum pressure within a closed system, the oscillation of the fluid particles provided a significant temperature gradient as it passes through the stack (Swift, 2001).

The thermoacoustic system is a simple system that only requires a driver or loudspeaker, a resonator and a stack. It requires no moving parts and can be obtained at a reasonable price with no refrigerant needed (Adeff and Hofler, 2000). Figure 1.1 shows the loudspeaker or transducer in the thermoacoustic engine, which is used to provide the acoustic power to the thermoacoustic system. The energy is then converted to the heat flux by the stack. This phenomenon is known as the thermoacoustic effect. A cold heat, Q_c is pumped from the cold reservoir to be cooled down by the cold heat exchanger. As for the hot heat, Q_h is released at the hot heat exchanger and therefore creating the temperature difference. (Marx et al., 2006).