

Faculty of Mechanical Engineering



Doctor of Philosophy

CHARACTERISATION OF KENAF/PINEAPPLE LEAF FIBRE REINFORCED COMPOSITE-METAL LAMINATES WITH ENHANCED MECHANICAL PROPERTIES

NG LIN FENG



UNIVERS Faculty of Mechanical Engineering

UNIVERSITI TEKNIKAL MALAYSIA MELAKA

DECLARATION

I declare that this thesis entitled "Characterisation of Kenaf/Pineapple Leaf Fibre Reinforced Composite-Metal Laminates with Enhanced Mechanical Properties" is the result of my own research except as cited in the references. The thesis has not been accepted for any degree and is not concurrently submitted in candidature of any other



degree.

APPROVAL

I hereby declare that I have read this thesis and in my opinion this thesis is sufficient in terms of scope and quality for the award of Doctor of Philosophy.

Signature Supervisor Name : ...Associate Professor Dr. Sivakumar Dhar Malingam..... Date . UNIVERSITI TEKNIKAL MALAYSIA MELAKA

DEDICATION

I would like to express my gratitude to my beloved father and mother for the continuous support and patient towards the completion of this thesis. Besides, I would like to give a special feeling of gratitude to my siblings who always motivate and support me from the beginning until the final stages of this research study. Once again, I would like to express

my deepest gratitude to those who have supported me throughout the process.



ABSTRACT

The mechanical properties of fibre metal laminates (FMLs) are worth investigating since such materials offer several superior characteristics over conventional metallic alloys. Majority of the research has focused on the mechanical properties of hybrid composite materials and conventional synthetic fibre-based FMLs. However, the mechanical properties of polypropylene-based short kenaf/pineapple leaf fibre reinforced hybrid composites and woven kenaf/pineapple leaf FMLs still remain unexplored. This study aims at investigating the influences of fibre weight compositions, chemical treatments and relative fibre ratios on the mechanical properties of non-hybrid and hybrid composites based on short kenaf/pineapple leaf fibres. In addition, the mechanical tests were performed to characterise the non-hybrid and hybrid woven kenaf/pineapple leaf fibrebased metal laminates with various fibre architectures and stacking configurations. In this research study, the kenaf/pineapple leaf fibre reinforced composites and FMLs were manufactured through the hot press moulding compression method. A series of mechanical tests were conducted to determine the mechanical properties of the materials. In accordance with the results obtained, the composites had evidenced the highest mechanical properties when the fibre weight composition was fixed at 30 wt% regardless of types of fibre. The mechanical properties of both kenaf and pineapple leaf fibre reinforced composites increased with the increase of fibre weight composition up to a critical limit of 30 wt %. The drop in the mechanical properties was noticed when the fibre weight composition was above the critical limit. In the context of chemical treatments, the NaOH and silane treated kenaf and pineapple leaf fibre-based composites showed higher mechanical properties over those of untreated composites. It was noticed that 5 % NaOH and 3 % silane treatments could provide excellent mechanical properties to the composite materials. However, the composites with the combination of the 5 % NaOH and 3 % silane treatments were shown to have the highest mechanical properties. When looking into the effect of hybridisation, the mechanical properties of the composites increased with the increase of pineapple leaf fibre content. Overall, the composites with the relative fibre ratio of 0 : 100 (kenaf : Pineapple leaf) evidenced the superior mechanical properties. When comparing the mechanical properties of FMLs with different fibre architectures, twill woven FMLs had outperformed those of plain woven FMLs irrespective of types of fibre. Furthermore, it was revealed that the hybrid pineapple leaf/kenaf/pineapple leaf fibrebased FMLs exhibited comparable mechanical and indentation properties to the non-hybrid pineapple leaf fibre-based FMLs particularly when subjected to out-of-plane loadings. Kenaf fibre has been shown to have high availability and economic value while pineapple leaf fibre is currently regarded as agricultural waste having high mechanical strength. Therefore, it can be concluded that the hybridisation of kenaf and pineapple leaf fibre in FMLs could develop a material with high economic value and mechanical strength while reducing the agricultural waste on the earth.

PENCIRIAN LAMINASI KOMPOSIT-LOGAM BERTETULANG SERAT KENAF/DAUN NANAS DENGAN SIFAT MEKANIKAL YANG DIPERTINGKATKAN

ABSTRAK

Sifat-sifat mekanikal serat bertetulang lamina logam (FMLs) penting untuk dikaji kerana bahan-bahan tersebut menawarkan beberapa ciri unggul berbanding dengan aloi logam konvensional. Kebanyakan penyelidikan telah memberi tumpuan pada sifat-sifat mekanikal bahan komposit hibrid dan FMLs konvensional berasaskan serat sintetik. Walau bagaimanapun, sifat-sifat mekanikal komposit hibrid kenaf/daun nanas pendek dan FMLs anyaman kenaf/daun nanas berasaskan polipropilena masih belum diterokai. Kajian ini bertujuan untuk menyiasat pengaruh komposisi berat serat, rawatan kimia dan nisbah serat relatif terhadap sifat-sifat mekanikal komposit bukan hibrid dan hibrid berasaskan serat kenaf/daun nanas pendek. Di samping itu, ujian-ujian mekanikal telah dilakukan untuk mencirikan lamina logam anyaman kenaf/daun nanas bukan hibrid dan hibrid dengan pelbagai seni bina serat dan konfigurasi serat. Dalam kajian ini, kenaf/daun nanas bertetulang komposit dan FMLs telah dihasilkan melalui kaedah pengacuan penekanan panas. Satu siri ujian mekanikal telah dijalankan untuk menentukan sifat-sifat mekanikal bahan-bahan. Selaras dengan keputusan yang diperolehi, komposit telah membuktikan sifat-sifat mekanikal tertinggi apabila komposisi berat serat ditetapkan pada 30 wt% tanpa mengira jenis serat. Sifat-sifat mekanikal kedua-dua kenaf dan serat daun nanas bertetulang komposit meningkat dengan peningkatan komposisi berat serat sehingga batas kritikal sebanyak 30 wt%. Pengurangan sifat-sifat mekanikal diperhatikan apabila komposisi berat serat melebihi batas kritikal. Dalam konteks rawatan kimia, komposit berasaskan serat kenaf dan daun nanas yang dirawat dengan NaOH dan silane menunjukkan sifat-sifat mekanikal yang lebih tinggi berbanding dengan komposit yang tidak dirawat. Ini telah diperhatikan bahawa rawatan dengan 5 % NaOH dan 3 % silane dapat memberikan sifat-sifat mekanikal yang sangat baik untuk bahan komposit. Walau bagaimanapun, komposit dengan kombinasi rawatan 5 % NaOH dan 3 % silane menunjukkan sifat-sifat mekanikal yang tertinggi. Apabila melihat pada kesan penghibridan, sifat-sifat mekanikal komposit meningkat dengan peningkatan kandungan serat daun nanas. Secara keseluruhannya, komposit dengan nisbah serat relatif 0 : 100 (kenaf : daun nanas) membuktikan sifat mekanikal yang unggul. Apabila membandingkan sifat-sifat mekanikal FMLs dengan seni bina serat yang berbeza, FMLs anyaman kelarai telah menunjukkan sifat-sifat mekanikal dan lekukan yang lebih tinggi daripada FMLs anyaman polos tanpa mengira jenis serat. Tambahan pula, ternyata FMLs serat daun nanas/kenaf/daun nanas hibrid menunjukkan sifat-sifat mekanikal dan lekukan yang setanding dengan FMLs serat daun nanas bukan hibrid terutamanya apabila mereka tertakluk kepada beban luar satah. Serat kenaf telah dibuktikan mempunyai ketersediaan dan nilai ekonomi yang tinggi manakala serat daun nanas kini dianggap sebagai sisa pertanian yang mempunyai kekuatan mekanikal yang tinggi. Oleh itu, ini dapat disimpulkan bahawa penghibridan serat kenaf dan daun nanas dalam FMLs boleh menghasilkan satu bahan yang mempunyai nilai ekonomi dan kekuatan mekanikal yang tinggi serta mengurangkan sisa pertanian di bumi.

ACKNOWLEDGEMENTS

First and foremost, I would like to show my deepest gratitude to my supervisor, Associate Professor Dr. Sivakumar Dhar Malingam for his patient guidance, support and encouragement from the initial to the final level of this project that enable me to gain a lot of theoretical knowledge and understanding throughout the overall process. In addition, he had also guided me to solve the problems faced during the research by suggesting other alternative ways. This project will not be successfully accomplished without his guidance and comment to improve the quality of this research study.

I would also like to express my sincere gratitude to my co-supervisor, Associate Professor Dr. Mohd Zulkefli Selamat for his theoretical support which allows me to complete this research within the given time. He had given me the experimental knowledge for conducting the test. Moreover, he had always given suggestions to me to perform experimental works successfully.

I owe my deepest gratitude to my parents and friends who had always given me mental support along the way. Their support acts as a power source to increase my determination to complete this project at my best. They always encouraged and believed in me that I could finish this project within the time given. Once again, I would like to thank those who made this thesis possible.

Last but not least, I would like to express my gratitude towards the Skim Zamalah UTeM for giving financial support.

TABLE OF CONTENTS

AP DE AB AC TA LIS LIS	PROV DICA STRA STRA STRA CKNO BLE ST OF ST OF ST OF	ATION ACT	i ii iv vii ix xiii xiv	
CH	[APT]	ER		
1.		RODUCTION	1	
	1.1	Background	1	
	1.2	Problem statement	5	
	1.3	Objectives	7	
	1.4	Scopes	8	
	1.5	Significance of the study	8	
	1.6	Thesis outline	11	
2.	LITERATURE REVIEW			
	2.1	Introduction	13	
	2.2	Fibre metal laminates	13	
	2.3	Composite materials	18	
		2.3.1 Hybrid composites	24	
		2.3.211 Matrix ITI TEKNIKAL MALAYSIA MELAKA	25	
		2.3.2.1 Thermoplastics and thermosets	26	
		2.3.2.2 Polypropylene	30	
		2.3.3 Reinforcements	35	
		2.3.3.1 Natural fibres	36	
		2.3.3.2 Kenaf fibre	45	
		2.3.3.3 Pineapple leaf fibre	49	
	2.4	Factors affecting FRP properties	51	
	2.5	Woven mats	57	
	2.6	Chemical treatments	61	
	2.7	Failure mechanism in FRPs	68	
	2.8	Adhesive bonding in FMLs	71	
	2.9	Review studies on mechanical properties	75	
		2.9.1 Review on mechanical properties of composites	76	
		2.9.2 Review on mechanical properties of FMLs	85	
	2.10	Summary	91	
3.	MAT	TERIALS AND METHODS	93	
	3.1	Introduction	93	

	3.2	aterial specifications 95			
	3.3	Material preparations			
	3.4	Composite preparations	96		
		3.4.1 Matrix	96		
		3.4.2 Reinforcement	98		
		3.4.2.1 Chemical treatments	99		
		3.4.2.2 Fabric cutting	100		
		3.4.2.3 Fibre drying	101		
		3.4.3 Compounding process	102		
		3.4.4 Composite fabrication process	104		
	Metallic alloy processing	108			
		3.5.1 Annealing process	108		
		3.5.2 Mechanical surface treatment	109		
	3.6	FML fabrication	111		
	3.7	Specimen preparation	112		
	3.8	Mechanical tests	113		
		3.8.1 Tensile test	114		
		3.8.2 Flexural test	114		
		3.8.3 Charpy impact test	115		
		3.8.4 Quasi-static indentation test	117		
	3.9	Morphological analysis	118		
	3.10	Summary	118		
4.		SULT AND DISCUSSION	120		
	4.1	Introduction	120		
	4.2	Effect of fibre weight composition	120		
		4.2.1 Tensile properties	121		
		4.2.2 Flexural properties	125		
		4.2.3 Impact properties	128		
	12	4.2.4 Morphological behaviour	132		
	4.3	Effect of chemical treatments AL MALAYSIA MELAKA	133		
		4.3.1 Tensile properties	134		
		4.3.2 Flexural properties	143		
		4.3.3 Impact properties	150		
	4 4	4.3.4 Morphological behaviour	157		
	4.4	Effect of relative fibre ratio	161		
		4.4.1 Tensile properties4.4.2 Flexural properties	162 164		
		4.4.2 Impact properties	167		
		4.4.4 Morphological behaviour	107		
	4.5		170		
	4.5	Effect of woven stacking configurations and architectures 4.5.1 Tensile properties	172		
		4.5.1 Flexural properties	175		
		4.5.2 Impact properties	181		
		4.5.4 Quasi-static indentation properties	181		
		4.5.5 Morphological behaviour	193		
	4.6	Summary	200		
	7.0	Summary	200		

5.	CONCLUSION AND RECOMMENDATIONS	205
	5.1 Conclusions	205
	5.2 Future recommendations	209
RE	EFERENCES	210
AP	PPENDIX	234



LIST OF TABLES

TITLE

PAGE

TABLE

2.1	Advantages and disadvantages of thermoplastics and thermosets	27
	(Joseph et al., 2003)	
2.2	Different sources of deriving propylene and their percentage (Aitani, 2006)	32
2.3	Comparison between glass fibre and natural fibres (Wambua et al., 2003)	36
2.4	Chemical compositions and microfibrillar angle of plant fibres (Dittenber and GangaRao, 2012)	39
2.5	Factors affecting the mechanical strength of plant fibres (Dittenber and GangaRao, 2012)	40
2.6	Physical and mechanical properties of plant fibres (Faruk et al., 2012)	41
2.7	Fibril size and the chemical composition of kenaf bast and core fibres (Wambua et al., 2003)	47
3.1	Compiled properties of the aluminium, reinforcements and matrix (Holbery, 2006; Dittenber et al., 2012; Atlas, 2013; Khan et al. 2018)	96
3.2	Short kenaf and PALF content in non-hybrid composites	103
3.3	Relative fibre ratios of short fibre reinforced hybrid composites with	103
	a total fibre content of 30 wt%	
3.4	Fibre weight fraction of composite laminates A MELAKA	107
3.5	Fibre volume fraction of composite laminates	108
3.6	Chemical composition of aluminium 5052 (Ng et al., 2017)	108
3.7	Average surface roughness (R _a) values of aluminium surfaces	110
3.8	ASTM and specimen dimension for each mechanical test	113
4.1	Tensile properties of kenaf fibre and PALF reinforced composites with varying fibre contents	122
4.2	Flexural properties of kenaf fibre and PALF reinforced composites with varying fibre contents	126
4.3	Impact properties of kenaf fibre and PALF reinforced composites with varying fibre contents in edgewise orientation	129
4.4	Impact properties of kenaf fibre and PALF reinforced composites with varying fibre contents in flatwise orientation	129
4.5	Tensile properties of 30 wt% kenaf fibre and PALF reinforced composites with varying chemical concentrations	135
4.6	Flexural properties of 30 wt% kenaf fibre and PALF reinforced composites with varying chemical concentrations	143

4.7	Impact properties of 30 wt% kenaf fibre and PALF reinforced composites with varying chemical concentrations in edgewise orientation	150
4.8	Impact properties of 30 wt% kenaf fibre and PALF reinforced composites with varying chemical concentrations in flatwise orientation	151
4.9	Tensile properties of non-hybrid and hybrid kenaf/PALF-based composites with different relative fibre ratios	162
4.10	Flexural properties of non-hybrid and hybrid kenaf/PALF-based composites with different relative fibre ratios	165
4.11	Impact properties of non-hybrid and hybrid kenaf/PALF-based composites with different relative fibre ratios in edgewise orientation	168
4.12	Impact properties of non-hybrid and hybrid kenaf/PALF-based composites with different relative fibre ratios in flatwise orientation	168
4.13	Tensile properties of plain and twill woven kenaf/PALF-based FMLs with different fibre stacking configurations	173
4.14	Flexural properties of plain and twill woven kenaf/PALF-based FMLs with different fibre stacking configurations	177
4.15	Impact properties of plain and twill woven kenaf/PALF-based FMLs with different fibre stacking configurations in edgewise orientation	182
4.16	Impact properties of plain and twill woven kenaf/PALF-based FMLs with different fibre stacking configurations in flatwise orientation	182
4.17	Indentation properties of plain and twill woven FMLs on 12.7 mm hemispherical indenter	186
4.18	Indentation properties of plain and twill woven-ply FMLs on 20 mm hemispherical indenter	187
	اونيۈمرسيتي تيكنيكل مليسيا ملاك	

UNIVERSITI TEKNIKAL MALAYSIA MELAKA

LIST OF FIGURES

FIGURE

TITLE

PAGE

2.1 Fibre bridging mechanism in FMLs (Khan et al., 2009)	15
2.2 Transition of fatigue crack period in FMLs (Homan, 2006)	16
2.3 Categories of FMLs based on the metallic skin layers and typ fibres	pes of 17
2.4 Polymer structure of thermoplastic and thermoset before and processing (Campbell, 2006)	l after 30
2.5 Propylene supply and demand from 2000 to 2020 (Akah and Ghrami, 2015)	Al- 32
2.6 Classification of thermoplastic polymers (Mohanty et al., 20	05) 34
2.7 Classification of natural and synthetic fibres (Sathishkumar (2014)	· ·
2.8 Chemical structure of cellulose in plant fibres (Gurunathan e 2015)	et al., 39
2.9 Relationship between vehicle weight reduction and carbon d emission (Ishikawa et al., 2018)	ioxide 42
2.10 Effect of moisture on the fibre-matrix adhesion (Azwa et al.,	2013) 44
2.11 Effect of reinforcement on the performance of the composite	· ·
materials (Campbell, 2010)	-
2.12 Types of woven mats (a) Unidirectional (b) Plain weave (c) weave (Cai et al., 2017)	Twill 60
2.13 Fibre structure (a) Untreated (b) NaOH treated (Mwaikambo Ansell, 2002)	and 64
2.14 Chemical interaction between silane and cellulosic fibres (X 2010)	ie et al., 65
2.15 Interaction between MAPP and cellulosic fibres (Pickering e 2016)	et al., 68
2.16 Different stages of crack growth in FRPs (Harris, 1999)	70
2.17 Damage development in woven mats (Lomov, 2008)	71
2.18 Interaction between MAPP, aluminium sheets and PP (a) Sn amount of MAPP (b) High amount of MAPP (Chen et al., 20	
2.19 Typical adhesive and cohesive failure of FMLs (Aghamohar et al., 2018)	,
2.20 Effect of surface roughness on the mechanical interlocking of metal-polymer (Lucchetta et al., 2011)	of 75
3.1 Flowchart of the research study	94
3.2 PP granules	97

2.2	Film stashing tashnisma	98	
3.3	Film stacking technique		
3.4	Short natural fibres (a) Kenaf (b) Pineapple leaf		
3.5	Woven fabrics (a) Plain weave (b) Twill weave		
3.6	Universal oven		
3.7	Haake Rheomix twin-screw internal mixer		
3.8	Fibre pellets (a) Kenaf (b) PALF		
3.9	Hydraulic hot press machine	105	
3.10	Processing temperature and pressure during composite fabrication	105	
3.11	Fibre stacking configurations in composite laminates	106	
3.12	Furnace with the temperature controller	109	
3.13	3D view of surface texture (a) Non-abraded (b) 80-gritsize	111	
3.14	FML with 2/1 stacking configuration	112	
3.15	Water jet cutting machine	112	
3.16	Specimens (a) Composites (b) FMLs	113	
3.17	Tensile test of the specimen	114	
3.18	3-point bending test of the specimen	115	
3.19	Charpy impact test of the specimen	116	
3.20	Impact orientations (a) edgewise (b) flatwise	117	
3.21	Setup of the quasi-static indentation test	118	
4.1	Stress-strain curves of kenaf fibre reinforced composites	124	
4.2	Stress-strain curves of PALF reinforced composites	124	
4.3	Load-displacement curves of kenaf fibre reinforced composites	127	
4.4	Load-displacement curves of PALF reinforced composites	127	
4.5	Impact strength of kenaf fibre reinforced composites in flatwise and	127	
4.3		151	
٨	edgewise orientations	131	
4.6	Impact strength of PALF reinforced composites in flatwise and	151	
47	edgewise orientations	120	
4.7	SEM micrograph of kenaf fibre reinforced composites at 30 wt%	132	
4.0	after fracture	100	
4.8	SEM micrograph of PALF reinforced composites at 30 wt% after	133	
4.0	US VERSITI TEKNIKAL, MALAYSIA MELAKA	100	
4.9	Stress-strain curves of kenaf fibre reinforced composites subjected	139	
	to NaOH treatment with varying concentrations		
4.10	Stress-strain curves of PALF reinforced composites subjected to	139	
	NaOH treatment with varying concentrations		
4.11	Stress-strain curves of kenaf fibre reinforced composites subjected	140	
	to silane treatment with varying concentrations		
4.12	Stress-strain curves of PALF reinforced composites subjected to	140	
	silane treatment with varying concentrations		
4.13	Comparison of the tensile properties of untreated and the	142	
	chemically-treated kenaf fibre reinforced composites		
4.14	Comparison of the tensile properties of untreated and the	142	
	chemically-treated PALF reinforced composites		
4.15	Load-displacement curves of kenaf fibre reinforced composites	145	
	subjected to NaOH treatment with varying concentrations		
4.16	Load-displacement curves of PALF reinforced composites subjected	146	
-	to NaOH treatment with varying concentrations	-	
4.17	Load-displacement curves of kenaf fibre reinforced composites	147	
	subjected to silane treatment with varying concentrations		

4 1 0		1 47
4.18	Load-displacement curves of PALF reinforced composites subjected to silane treatment with varying concentrations	147
4.19	Comparison of the flexural properties of untreated and the	149
т.17	chemically-treated kenaf fibre reinforced composites	177
4.20	Comparison of the flexural properties of untreated and the	149
	chemically-treated PALF reinforced composites	117
4.21	Impact strength of kenaf fibre reinforced composites subjected to	152
1.21	NaOH treatment with varying concentrations	152
4.22	Impact strength of PALF reinforced composites subjected to NaOH	152
	treatment with varying concentrations	
4.23	Impact strength of kenaf fibre reinforced composites subjected to	154
	silane treatment with varying concentrations	
4.24	Impact strength of PALF reinforced composites subjected to silane	154
	treatment with varying concentrations	
4.25	Comparison of the impact strength of untreated and the chemically-	156
	treated kenaf fibre reinforced composites	
4.26	Comparison of the impact strength of untreated and the chemically-	156
	treated PALF reinforced composites	
4.27	SEM images of the kenaf fibre surfaces (a) 1 % NaOH (b) 3 %	158
	NaOH (c) 5 % NaOH (d) 7 % NaOH (e) untreated	
4.28	SEM images of the PALF surfaces (a) 1 % NaOH (b) 3 % NaOH	159
	(c) 5 % NaOH (d) 7 % NaOH (e) untreated	
4.29	Fractographic images of 5 % NaOH treated composites (a) Kenaf	161
4.00	(b) PALF	1 < 1
4.30	Fractographic images of 3 % silane treated composites (a) Kenaf	161
4 21	(b) PALF	162
4.31	Stress-strain curves of non-hybrid and hybrid kenaf/PALF-based composites with different relative fibre ratios	163
4.32	Load-displacement curves of non-hybrid and hybrid kenaf/PALF-	166
4.52	based composites with different relative fibre ratios	100
4.33	Comparison of the impact strength of non-hybrid and hybrid	169
1.55	kenaf/PALF-based composites with different relative fibre ratios	107
4.34	SEM micrograph of non-hybrid and hybrid kenaf/PALF composites	171
	after fracture (a) 100 : 0 (b) 0 : 100 (c) 75 : 25 (d) 50 : 50 (e) 25 : 75	
4.35	Stress-strain curves of non-hybrid and hybrid plain woven	174
	kenaf/PALF FMLs	
4.36	Stress-strain curves of non-hybrid and hybrid twill woven	174
	kenaf/PALF FMLs	
4.37	Load-displacement curves of non-hybrid and hybrid plain woven	178
	kenaf/PALF FMLs	
4.38	Load-displacement curves of non-hybrid and hybrid twill woven	178
	kenaf/PALF FMLs	
4.39	Impact strength of non-hybrid and hybrid plain woven kenaf/PALF	183
	FMLs	
4.40	Impact strength of non-hybrid and hybrid twill woven kenaf/PALF	183
4 4 4	FMLs	100
4.41	Indentation force-displacement curves of non-hybrid and hybrid	188
	plain woven kenaf/PALF FMLs on 12.7 mm hemispherical indenter	

4.42	Indentation force-displacement curves of non-hybrid and hybrid	188
	twill woven kenaf/PALF FMLs on 12.7 mm hemispherical indenter	
4.43	Indentation force-displacement curves of non-hybrid and hybrid	191
	plain woven kenaf/PALF FMLs on 20 mm hemispherical indenter	
4.44	Indentation force-displacement curves of non-hybrid and hybrid	191
	twill woven kenaf/PALF FMLs on 20 mm hemispherical indenter	
4.45	SEM micrograph of plain woven kenaf/PALF FMLs after fracture	193
	(a) [K/K/K] (b) [K/P/K] (c) [P/K/P] (d) [P/P/P]	
4.46	SEM micrograph of twill woven kenaf/PALF FMLs after fracture	194
	(a) [K/K/K] (b) [K/P/K] (c) [P/K/P] (d) [P/P/P]	
4.47	Optical images of plain woven kenaf/PALF FMLs after indentation	196
	test on 12.7 mm hemispherical indenter	
4.48	Optical images of twill woven kenaf/PALF FMLs after indentation	197
	test on 12.7 mm hemispherical indenter	
4.49	Optical images of plain woven kenaf/PALF FMLs after indentation	198
	test on 20 mm hemispherical indenter	
4.50	Optical images of twill woven kenaf/PALF FMLs after indentation	199
	test on 20 mm hemispherical indenter	



LIST OF SYMBOLS AND ABBREVIATIONS

ARALL	-	Aramid reinforced aluminium laminate
ASTM	-	American society for testing and material
CARALL	-	Carbon fibre reinforced aluminium laminate
CCCs	-	Carbon-carbon composites
CMCs	-	Ceramic matrix composites
D	-	Diameter
E_A	-	Total absorbed energy
E_f	-	Flexural modulus
$\dot{E_T}$	-AALAYSI	Impact strength
F	24-	Flexural force
FCC	S -	Fluid catalytic cracking
FMLs	¥ -	Fibre metal laminates
FRPs	F _ ==	Fibre reinforced polymers
GLARE	E - =	Glass fibre reinforced aluminium laminate
IMCs	· · · · · · · · · · · · · · · · · · ·	Intermetallic matrix composites
Κ	1/wn :	Woven kenaf fabric
L	A = (Support span
L_c	2No hun	Critical fibre length
m		Slope of the load-displacement curve
MMCs	UNIVERSIT	Metal matrix composites
n	UNIVERSI	Number of woven fibre fabrics in the laminate
NaOH	-	Sodium hydroxide
Р	-	Woven pineapple leaf fabric
PALF	-	Pineapple leaf fibre
$ ho_c$	-	Density of composite laminate
$ ho_f$	-	Fibre density
PMCs	-	Polymer matrix composites
PP	-	Polypropylene
R _a	-	Surface roughness value
t	-	Thickness
$ au_y$	-	Shear strength
σ_{f}	-	Flexural strength
σ_{fibre}	-	Ultimate tensile strength of fibre
V_f	-	Fibre volume fraction
W	-	Width
W _c	-	Composite weight
W_f	-	Fibre weight fraction
W_{ff}	_	Fibre weight
••))		xiii
		A111

LIST OF PUBLICATIONS

Journals

- Ng, L.F., Malingam, S.D., Ishak, N.M., Kathiravan, S., 2020. Novel Sandwich Structure of Composite-Metal Laminates based on Cellulosic Woven Pineapple Leaf Fibre. *Journal of Sandwich Structures & Materials*. (Published Manuscript; Scopus/ISI; Q1/Q1; IF: 5.616)
- Ng, L.F., Malingam, S.D., Chen, W.P., 2020. The Effects of Woven Architectures and Stacking Configurations on the Mechanical and Indentation Properties of Kenaf/PALF Reinforced Metal Laminates. *Journal of Reinforced Plastics and Composites*. (Published Manuscript; Scopus/ISI; Q1/Q1; IF: 1.987)
- Ng, L.F., Malingam, S.D., Razali, N., Subramonian, S., 2020. Alkali and Silane Treatments towards Exemplary Mechanical Properties of Kenaf and Pineapple Leaf Fibre-reinforced Composites. *Journal of Bionic Engineering*, 17, pp. 380–392. (Published Manuscript; Scopus/ISI; Q2/Q2; IF: 2.222)
- Ng, L.F., Malingam, S.D., Chen, W.P., and Razali, N., 2019. Mechanical Properties and Water Absorption of Kenaf/Pineapple Leaf Fibre Reinforced Polypropylene Hybrid Composites. *Polymer Composites*, pp. 1–10. doi: 10.1002/pc.25451 (Published Manuscript; Scopus/ISI; Q2/Q2; IF: 2.265)

- Ng, L.F., Malingam, S.D., Woo, X.J., Kathiravan, S., and Siva, I., 2019. The Effects of Bonding Temperature and Surface Roughness on the Shear Strength of Bonded Aluminium Laminates using Polypropylene based Adhesive. *Journal of Advanced Manufacturing Technology*, 13(2), pp. 113–127. (Published Manuscript; Scopus; Q3; IF: 0.173)
- Ng, L.F., Malingam, S.D., Selamat, M.Z., Mustafa, Z., and Bapokutty, O., 2019. A Comparison Study on the Mechanical Properties of Composites based on Kenaf and Pineapple Leaf Fibres. *Polymer Bulletin*, 77, pp. 1449–1463. doi: 10.1007/s00289-019-02812-0 (Published Manuscript; Scopus/ISI; Q2/Q2; IF: 2.014)
- Ng, L.F., Malingam, S.D., Jenal, R., Mustafa, Z., and Subramonian, S., 2018. A Review of the Tensile and Fatigue Responses of Cellulosic Fibre-Reinforced Polymer Composites. *Mechanics of Advanced Materials and Structures*, 27(8), pp. 645–660. doi: 10.1080/15376494.2018.1489086 (Published Manuscript; Scopus/ISI; Q1/Q1; IF: 3.517)

UNIVERSITI TEKNIKAL MALAYSIA MELAKA

Book chapter

Ng, L.F., and Malingam, S.D., 2019. Monotonic and Fatigue Responses of Fiber-Reinforced Metal Laminates, In: Jawaid, M., Thariq, M., and Saba, N. (eds) *Mechanical and Physical Testing of Biocomposites, Fibre-Reinforced Composites and Hybrid Composites*, pp. 307–323. Cambridge: Woodhead Publishing.

CHAPTER 1

INTRODUCTION

1.1 Background

During the past few decades, the enormous evolution of technology has aroused the development of new categories of metal-composite hybrid materials, namely Fibre Metal Laminates (FMLs). The FMLs concept is based on the synthesis of metallic skin layers and composite materials as the core constituent. FMLs are considered as the sandwich materials that are formed by consolidating the monolithic metallic alloys to the composite materials by means of adhesive agents. Over the years, it has been demonstrated that FMLs possess several superior advantages over those of monolithic metal and composite materials. Indeed, the main purpose of combining the constituents of metallic alloys and composite materials is to remedy the obstacle of the poor fatigue resistance of the monolithic aluminium alloys (Ferrante et al., 2016). The metal-composite interfaces allow effective energy dissipation and retard the rapid crack growth propagation through the fibre bridging mechanism, thus, improving the resistance of the materials against cyclic loading (Alderliesten, 2015). Although the initial intention of developing FMLs is to tackle the poor fatigue resistance of monolithic aluminium alloys, however, it was found that the metal-composite interfaces play an important role in dissipating energy, having an excellent impact resistance as well. It should be highlighted that the partial substitution of metallic alloys with composite materials in FMLs leads to significant overall weight reduction, resulting in low energy consumption (Chai and Manikandan, 2014; Sivakumar

et al., 2017). The achievement in FMLs has continuously motivated the research communities to explore the mechanical properties of FMLs with different concepts. Due to the outstanding advantages in FMLs, these sandwich materials have gained wide acceptance as an alternative structural material to substitute the monolithic aluminium alloys, particularly in aerospace industries in order to ensure structural integrity and safety performance.

In aerospace industries, FMLs are considered as a part of the third evolution materials to further improve the aerospace efficiency without deteriorating the safety performance. FMLs that combine the advantages inherited from their respective composite materials and metallic alloys are currently being used as fuselage materials. The first generation of aircraft materials is exemplified by the wooden materials in the year 1903 when the Wright brothers, who are the inventors of the aeroplane, successfully develop the first aeroplane in the world using spruce wood as the construction materials. Wooden materials have gained widespread usage due to their high availability and low-cost characteristic. Environmental impacts such as high moisture uptake, termite attacks and degradation after a certain period are those of the disadvantages of employing wooden materials as the construction components. The second generation of aircraft materials is represented by aluminium alloys which were used to replace wood as the essential components in aircraft structures in the year 1930. In the 1930s, the aluminium alloy was employed for the construction of Douglas C-47 military transport aircraft. Owing to the high strength to weight ratio characteristic of aluminium alloys, they have been widely employed in the aircraft industries for structural applications. However, the evolution of the technology has inclined towards the utilisation of composite materials in aircraft industries in the 1990s. The composite materials can be tailored to achieve the specific

mechanical properties by the proper selection of fibre types, fibre orientation and stacking configurations to fulfil the structural requirement for aircraft components.

The commercially available FMLs are glass fibre reinforced aluminium laminate (GLARE), Aramid fibre reinforced aluminium laminate (ARALL) and Carbon fibre reinforced aluminium laminate (CARALL). The first generation of FMLs is ARALL, consisting of aramid fibre reinforced epoxy composites bonded to the aluminium skin layers. ARALL was successfully developed at the Faculty of aerospace engineering of the Delft University of Technology (TU Delft) in 1978 (Villanueva and Cantwell, 2004). It has been demonstrated that ARALL possesses excellent fatigue crack resistance over the monolithic aluminium. To further improve the mechanical strength of FMLs, high strength carbon fibre was incorporated in FMLs instead of aramid fibre. However, carbon fibre exhibited poor fatigue resistance due to fibre failure during the fatigue test at elevated stress levels (Sinmazcelik et al., 2011). Due to the disadvantages of carbon fibre, glass fibre as an alternative reinforcement was introduced into FMLs in 1990 to improve the properties (Ammar et al., 2019).

The alternate stack configuration in FMLs has offered excellent damage tolerance and fatigue crack resistance via the fibre bridging mechanism (Zhou et al., 2015). Due to the combination of advantages in metallic alloy and composite materials, the strength and durability of the materials have been drastically improved. The relatively low fatigue crack growth rate of FMLs compared to monolithic aluminium is particularly vital for the mechanical structures as the inspection interval of the structures can be increased, which directly avoids the secondary damage to other components. Because of the excellent mechanical properties of FMLs, the applications of FMLs have been further extended to various fields and they are currently being proposed in the automotive field to improve vehicle efficiency. Apart from that, the stringent environmental rules and regulations aligned with the increasing environmental awareness and consciousness have inspirited the researcher to search for lightweight materials to reduce energy consumption as well as contaminant emission. Reducing vehicle weight is one of the known techniques that could be applied to reduce the energy consumption and harmful contaminant of a vehicle. Since FMLs are lighter than metallic alloys, introducing the FMLs into manufacturing of vehicle components leads to the overall weight reduction, resulting in less fuel consumption and less contaminant emission. Hence, the overall vehicle efficiency is undoubtedly enhanced.

The composite materials indeed have a major contribution to the mechanical properties of FMLs. Fibre types, fibre orientation and fibre configurations are factors influencing the mechanical properties of FMLs. The demand for composite materials has been continuously increasing in almost every branch of engineering applications since the past few decades, from the aircraft industries to the automotive industries. The advent of composite materials in various applications could be due to their outstanding advantages such as high specific mechanical properties and excellent heat and corrosion resistance (Arju et al., 2015). However, the most commonly available composite materials that have been widely used are based on synthetic fibres, particularly with glass fibre. Before the development of FMLs, metallic alloys and composite materials were two favourite materials that were being used in aircraft industries. Nevertheless, both materials exhibited disadvantages such as poor impact resistance and residual strength in composite materials and low fatigue resistance in metallic alloys. Therefore, an attempt to combine these two competing materials had been successfully conducted to remedy their respective shortcomings. As a result, FMLs with excellent performance had been developed, which play an important role in improving the efficiency and performance of vehicle and aircraft.