



**Faculty of Mechanical Engineering**

A large, faded version of the UTeM logo is centered in the background of the page. It includes the circular emblem, the 'UTeM' text box, the Arabic name, and the full name in English.

**INVESTIGATION OF MECHANICAL PERFORMANCE OF WOVEN  
KENAF/GLASS HYBRID COMPOSITE METAL LAMINATE**

**Kathiravan S/O Subramaniam**

**Master of Science in Mechanical Engineering**

**2021**

**INVESTIGATION OF MECHANICAL PERFORMANCE OF WOVEN  
KENAF/GLASS HYBRID COMPOSITE METAL LAMINATE**

**KATHIRAVAN S/O SUBRAMANIAM**

**A thesis submitted  
in fulfillment of the requirements for the degree of Master of Science in Mechanical  
Engineering**



**UNIVERSITI TEKNIKAL MALAYSIA MELAKA**

**2021**

## DECLARATION

I declare that this thesis entitled “Investigation of Mechanical Performance of Woven Kenaf/Glass Hybrid Composite Metal Laminate” is the result of my own research except as cited in the references. The thesis has not been accepted for any degree and is not concurrently submitted in candidature of any other degree.



## APPROVAL

I hereby declare that I have read this thesis and in my opinion this thesis is sufficient in terms of scope and quality for the award of Master of Science in Mechanical Engineering.

 Signature	:	.....
Supervisor Name	:	Ts. Dr. Omar Bin Bapokutty
Date	:	.....

اونيورسيتي تيكنيكل مليسيا ملاك

UNIVERSITI TEKNIKAL MALAYSIA MELAKA

## DEDICATION

To my beloved family and friends.



## ABSTRACT

In the past few decades, research and engineering interests have been shifting from monolithic materials to fibre reinforced polymer materials. The biggest advantage of composite materials is that they are lightweight as well as tough. By choosing the suitable combination of matrix and reinforcement, a new material can be produced that meets the requirements of a particular application. In order to improve the properties of existing composites, new research leads to the development of Fibre Metal Laminate (FML). Fibre Metal Laminates (FML) is a class of hybrid structure formed from the combination of thin metal layers and fibre reinforced composites bonded together. The increasing of environmental concerns and the need for high-performance materials lead to the development of natural and synthetic hybrid composites. Hybridization of natural and synthetic fibres in single matrix results in the enhancement of mechanical properties of the composite by taking the best advantages of one fibre to overcome the disadvantage of another fibre which consequently minimize the dependent on synthetic fibres. This work presents the effects of fibre stacking configuration on tensile and quasi-static indentation (QSI) and low-velocity impact (LVI) on kenaf/glass hybrid fibre metal laminates (FML). Two different hybrid stacking configurations of kenaf/glass metal laminates reinforced with polypropylene matrix were prepared through a hot compression process. Non-hybrid kenaf and glass metal laminates were also prepared for comparison. A tensile test was conducted according to ASTM E8, a QSI test was conducted according to ASTM D 6264 using 12.7 mm and 20 mm hemispherical indenters while an LVI test was conducted in accordance with ASTM D 7136. The tensile fractured surface of FML laminates was examined using scanning electron microscopy (SEM) while optical micrograph was used to investigate the failure mechanism of quasi-statically penetrated laminates. From the results, FMLs with the glass plies at the outer layers of composite [G/K<sub>2</sub>/G] showed a positive hybrid effect as they displayed better tensile, penetration and impact resistance, compared to the non-hybrid kenaf and glass reinforced FMLs. For tensile test, [G/K<sub>2</sub>/G] hybrid FML able to withstand higher strength compared to non-hybrid glass FML composites while for quasi-static indentation (QSI) test, [G/K<sub>2</sub>/G] hybrid FML exhibit highest penetration load and energy absorption followed by non-hybrid glass FML [G<sub>3</sub>], [K<sub>2</sub>/G/K<sub>2</sub>] and lastly [K<sub>6</sub>]. Similar behaviour is noticed as QSI, [G/K<sub>2</sub>/G] hybrid FML display good impact resistance in overall. It was observed that the overall performance of FML laminates decreases as the kenaf content in laminates increases. The potential of kenaf/glass hybrid FMLs in tolerating impact loads is evident. Thus hybrid structure can be used for impact loading applications while reducing the dependence on synthetic fibres. Overall, this study is an exploration of the potential applications of metal laminates reinforced with natural and synthetic fibre.

## **KAJIAN PRESTASI MEKANIKAL KENAF TERJALIN / KACA HIBRID RENCAM LAMINA LOGAM**

### **ABSTRAK**

*Sejak beberapa dekad yang lalu, kepentingan penyelidikan dan kejuruteraan telah beralih dari bahan-bahan monolitik ke bahan polimer diperkuat gentian. Manfaat terbesar bahan komposit adalah ringan serta keras. Dengan memilih kombinasi yang sesuai matriks dan peneguhan, satu bahan baru boleh dihasilkan dengan memenuhi keperluan-keperluan satu penggunaan tertentu. Bagi meningkatkan sifat komposit sedia ada, penyelidikan baru membawa ke pembangunan Gentian Logam Berlamina (FML). Gentian Logam Berlamina (FML) ialah satu kelas struktur hibrid dibentuk dari gabungan lapisan-lapisan logam nipis dan gentian komposit yang diperteguhkan mengikat bersama. Peningkatan tahap kesedaran alam sekitar dan keperluan untuk bahan-bahan prestasi tinggi menjurus kepada pembangunan hibrid semula jadi dan komposit hybrid bersintetik. Penghibridan gentian sintetik dan semula jadi dalam matriks tunggal mengakibatkan peningkatan sifat mekanik rencam dengan mengambil manfaat terbaik satu gentian mengatasi kekurangan satu lagi gentian yang mana meminimalkan kebergantungan gentian sintetik. Kerja ini membentangkan kesan konfigurasi tindanan gentian terhadap tegangan dan lekukan-statik (QSI) dan kesan hentamam halaju rendah (LVI) pada kenaf / gentian hibrid kaca berlamina logam. Dua hibrid berbeza konfigurasi tindanan kenaf lamina logam / kaca dikukuhkan dengan matriks polipropilena telah disediakan melalui proses mampatan panas. Kenaf bukan hibrid dan lamina logam kaca juga disediakan untuk perbandingan. Ujian tegangan dijalankan mengikut ASTM E8 dan ujian QSI mengikut ASTM D 6264 menggunakan pelekuk hemisfera dimensi 12.7 mm dan 20 mm. Ujian LVI dijalankan selaras dengan ASTM D 7136. Permukaan patah tegangan lamina FML diperiksa menggunakan mikroskop elektron imbasan manakala mikrograf optik digunakan untuk menyiasat mekanisme kegagalan kuasi-statik penembusan lamina. Satu kesan hibrid positif dalam  $[K_2/G/K_2]$  FML dengan lapisan kenaf diantara lapisan kaca serta dilapisi logam menunjukkan tegangan, QSI dan rintangan hentaman lebih baik daripada kenaf bukan hibrid dan kaca diperkukuhkan lamina FML. Dapat dilihat bahawa prestasi keseluruhan lamina FML berkurang apabila kandungan kenaf dalam lamina bertambah. Keseluruhan, kajian ini ialah satu penjelajahan mengenai potensi kegunaan untuk lamina logam diperkukuhkan dengan gentian sintetik dan semula jadi.*

## ACKNOWLEDGEMENTS

First and foremost, I would like to take this opportunity to express my sincere gratitude to my supervisor Ts. Dr. Omar Bin Bapokutty for his nonstop supervision, support, motivation, encouragement, and immense knowledge towards the completion of research and thesis writing.

I would also like to express my gratitude to Associate Professor Dr. Sivakumar Dhar Malingam as co-supervisor of this project for his unlimited advice and suggestions. Also, to my deepest thanks to the Ministry of Education Malaysia for supporting this research by the grant (Grant No.: FRGS/1/2015/SG06/FKM/03/F00276).

I would also like to express my deepest gratitude to Ng Lin Feng, for his contribution on giving ideas and all the technicians from the laboratory Faculty of Mechanical Engineering for their assistance and efforts in the entire lab and analysis works.

Special thanks to my family and friends for their moral support in completing this project. Lastly, thank you to everyone who are not listed here who had been to the crucial parts of realization of this project.

## TABLE OF CONTENTS

	PAGE
<b>DECLARATION</b>	
<b>APPROVAL</b>	
<b>DEDICATION</b>	
<b>ABSTRACT</b>	<b>i</b>
<b>ABSTRAK</b>	<b>ii</b>
<b>ACKNOWLEDGEMENTS</b>	<b>iii</b>
<b>TABLE OF CONTENTS</b>	<b>iv</b>
<b>LIST OF TABLES</b>	<b>vi</b>
<b>LIST OF FIGURES</b>	<b>vii</b>
<b>LIST OF APPENDICES</b>	<b>xii</b>
<b>LIST OF ABBREVIATIONS</b>	<b>xiii</b>
<b>LIST OF PUBLICATIONS</b>	<b>xv</b>
<b>CHAPTER</b>	
<b>1. INTRODUCTION</b>	<b>1</b>
1.1 Background	1
1.2 Problem statement	5
1.3 Objectives	7
1.4 Scope	7
1.5 Thesis structure	9
<b>2. LITERATURE REVIEW</b>	<b>11</b>
2.1 Introduction	11
2.2 Fibre metal laminate (FML)	11
2.3 Composite	14
2.3.1 Fibre-reinforced composite (FRP)	16
2.3.2 Matrix	17
2.3.2.1 Thermoplastic And Thermoset	17
2.3.3 Reinforcement	20
2.3.3.1 Synthetic Fibre	21
2.3.3.2 Natural Fibre	23
2.4 Factors affect the FRP strength	31
2.5 Woven structure	32
2.6 Hybrid composite structure	34
2.7 Low-velocity impact test (LVI)	36
2.8 Quasi-static indentation test (QSI)	39
2.9 Tensile test on FRP	41
2.10 QSI test on FRP	43
2.11 LVI test on FRP	47
2.12 Tensile test on FML	50
2.13 QSI on FML	51
2.14 LVI on FML	53
2.15 Concluding remarks	60
<b>3. METHODOLOGY</b>	<b>62</b>
3.1 Introduction	62

3.2	FML panel manufacturing and testing flow chart	62
3.3	Materials	63
3.3.1	Kenaf bast fibre	63
3.3.2	Woven E-glass	64
3.3.3	Maleic anhydride polypropylene (MAPP)	64
3.3.4	Polypropylene (PP)	65
3.3.5	Aluminium	68
3.4	Composite stacking configuration	70
3.5	Composite and FML fabrication	71
3.5.1	Composite fabrication	71
3.5.2	FML fabrication process	73
3.6	Specimen preparation	74
3.7	Tensile test	75
3.8	Quasi-static indentation test	77
3.9	Low-velocity impact (LVI) test	79
3.10	Damage morphology	82
<b>4.</b>	<b>RESULT AND DISCUSSION</b>	<b>83</b>
4.1	Introduction	83
4.2	Tensile test results	83
4.2.1	Failure analysis	85
4.3	Quasi-static indentation test results	86
4.3.1	Quasi-static indentation test using 12.7 mm hemispherical indenter	87
4.3.2	Quasi-static indentation test using 20 mm hemispherical indenter	96
4.3.3	Comparison of quasi-static indentation test using 12.7 mm and 20 mm hemispherical indenter	102
4.4	Low-velocity impact test results (12.7 mm hemispherical indenter)	103
4.4.1	Load-displacement curves of kenaf/glass hybrid and non-hybrid FML laminates	104
4.4.2	Load-time curves of kenaf/glass hybrid and non-hybrid FML laminates	109
4.4.3	Failure analysis	114
4.5	Summary	119
<b>5.</b>	<b>CONCLUSION AND RECOMMENDATIONS FOR FUTURE RESEARCH</b>	<b>123</b>
5.1	Conclusion	123
5.2	Recommendations	124
	<b>REFERENCES</b>	<b>125</b>
	<b>APPENDICES</b>	<b>148</b>

## LIST OF TABLES

<b>TABLE</b>	<b>TITLE</b>	<b>PAGE</b>
2.1	Comparison between thermoset and thermoplastic (Arnold et al., 1992)	18
2.2	Mechanical properties of PP (Maddah, 2016)	19
2.3	Comparison between natural and synthetic fibres	21
2.4	Mechanical and chemical properties of natural fibres (Ramesh, 2016)	26
2.5	Impact classification according to impact energy (Tan and Akil, 2012)	58
3.1	PP and MAPP composition for each cycle	66
3.2	HAAKE Rheomex OS single screw extruder parameters for the polymer compounding process	67
3.3	Chemical composition of aluminium 5052-H32 (Jeon et al., 2014)	69
3.4	Composition of composite laminates	73
3.5	Specifications of the impact tests carried out on FML laminates	80
4.1	Average values of tensile strength and tensile modulus for kenaf/glass FML	84
4.2	Maximum penetration load and energy absorbed by kenaf/glass hybrid and non-hybrid FML laminates by a 12.7 mm hemispherical indenter	90
4.3	Maximum penetration load and energy absorbed by kenaf/glass hybrid and non-hybrid FML laminates by a 20 mm hemispherical indenter	99
4.4	Impact parameter and results obtained from the low velocity impact test for each kenaf/glass hybrid and non-hybrid FML laminate	112

## LIST OF FIGURES

FIGURE	TITLE	PAGE
1.1	A sample lay-up of FML	1
2.1	Illustration of a sample fibre metal laminate (Dharmalingam et al., 2009)	12
2.2	Polypropylene structure (Maddah, 2016)	19
2.3	Classification of natural (Ramesh, 2016)	24
2.4	Woven kenaf bast fibre	27
2.5	(a) longitudinal view of the untreated kenaf fibres (b) SEM images of the cross section of kenaf fibre (Aziz and Ansell, 2004; Shibata et al., 2008)	28
2.6	Fiber bundle tensile strength of differently treated kenaf fiber— (Source: Edeerozey et al., 2007)	29
2.7	SEM micrograph of (a) an untreated kenaf fibre and (b) 3% NaOH treated kenaf fibre (Edeerozey et al., 2007)	30
2.8	Tensile specimens for kenaf fibres (Ochi, 2008)	31
2.9	Warp and weft pattern	33
2.10	Different types of weave	34
2.11	Typical force-displacement curve of quasi-static indentation (Bulut and Erkgig, 2018)	41

2.12	Force displacement curve for Kevlar/epoxy composites (Yahaya et al., 2014c)	45
2.13	Optical pictures of damaged surface of hybrid composite laminates after quasi-static test, cross-sectional surface, rear surface, and impacted surface: (a) Kevlar composite, (b) hybrid of placing kenaf layers and Kevlar 29 layers separately, (c) hybrid of placing kenaf layers alternately with Kevlar 29 layers and (d) kenaf composite (Suhad et al., 2017)	47
2.14	Impact damage of different view for glass/carbon and carbon/glass hybrid composite after subjected to impact test (Sayer et al., 2010)	50
2.15	Photographs of the indented: (a) pure kenaf fibre plate, (b) 2/1-0.3 FMLs, (c) 2/1-0.6 FMLs and (d) 3/2-0.6 FMLs (Abdullah et al., 2014)	52
2.16	Photographs of the indented 3/2 FMLs (Pang et al., 2015)	53
2.17	Typical load–displacement curve following a low velocity impact test on a FML (Carrillo and Cantwell, 2009)	55
2.18	Cross-sections of four scaled specimens impacted (Carrillo and Cantwell, 2009)	56
2.19	Absorbing energy vs impact energy (Múgica et al., 2012)	56
2.20	Cross section of the impacted plate (Múgica et al., 2012)	57
2.21	Schematic diagram of a sandwich structure configuration (Tan and Akil, 2012)	58
2.22	Maximum peak load under various impact energy levels (Tan and Akil, 2012)	59

2.23	Absorbed energy on composite specimen under various impact energy (Tan and Akil, 2012)	59
2.24	Side view of damaged specimen (Tan and Akil, 2012)	60
3.1	Flow chart on FML panel manufacturing and testing processes	63
3.2	Plain woven kenaf bast fibre	64
3.3	Plain woven glass fibre	64
3.4	HAAKE Rheomex OS single screw extruder	66
3.5	Plastic granulator	68
3.6	Fabricated modified PP sheet	68
3.7	Stacking configuration of composites “G” and “K” correspond to woven glass and kenaf fibre plies respectively	71
3.8	Compression moulding machine	72
3.9	FML layup	74
3.10	Schematic diagram and dimension of the specimen for QSI and LVI testing	75
3.11	Tensile test setup using INSTRON 8872 servohydraulic universal testing machine	76
3.12	Schematic diagram and dimensions of the specimen for the tensile test	76
3.13	Quasi-static indentation test setup	78
3.14	Schematic illustration of the quasi-static indentation fixture	78
3.15	Schematic diagrams of test specimens on edge supported configuration, indented using hemispherical indenters (a) 12.7 mm in diameter and (b) 20 mm in diameter	79
3.16	INSTRON CEAST 9340 drop tower impact tester	81

3.17	(a) close-up view of the impact test support fixture and (b) hemispherical tip indenter (12.7mm in diameter)	81
3.18	JEOL-6010 PLUS scanning electron microscope (SEM)	82
4.1	Tensile properties of FML laminate	85
4.2	SEM micrograph of fractured FML laminates after tensile test: (a) [G/K <sub>2</sub> /G], (b) [G <sub>3</sub> ], (c) [K <sub>2</sub> /G/K <sub>2</sub> ] and (d) [K <sub>6</sub> ]	86
4.3	Load-displacement curves of kenaf/glass hybrid and non-hybrid FMLs penetration by a 12.7 mm hemispherical indenter	87
4.4	Maximum penetration load of kenaf/glass hybrid and non-hybrid FML laminates by a 12.7 mm hemispherical indenter	89
4.5	Maximum penetration energy of kenaf/glass hybrid and non-hybrid FML laminates by a 12.7 mm hemispherical indenter	90
4.6	Optical image of damaged surface on FML laminates after the quasi-static perforation test using a 12.7 mm indenter	94
4.7	Crack propagation on the rear surface of [G/K <sub>2</sub> /G] FML laminate during the quasi-static penetration test using a 12.7 mm hemispherical indenter	95
4.8	Cross-sectional view of FML laminates after the quasi-static penetration test using a 12.7 mm hemispherical indenter: (a) [G/K <sub>2</sub> /G] and (b) [K <sub>6</sub> ]	95
4.9	Load-displacement curves of kenaf/glass hybrid and non-hybrid FMLs penetration by a 20 mm hemispherical indenter	96
4.10	Maximum penetration energy of kenaf/glass hybrid and non-hybrid FML laminates by a 20 mm hemispherical indenter	98

4.11	Maximum penetration load of kenaf/glass hybrid and non-hybrid FML laminates by a 20 mm hemispherical indenter	98
4.12	Optical image of damaged surface on FML laminates after the quasi-static perforation test using a 20 mm indenter	101
4.13	Sample cross-section view of [G/K <sub>2</sub> /G] FML laminates subjected to quasi-static loading by indenters measuring (a) 12.7 mm and (b) 20 mm	101
4.14	Maximum penetration load and energy of kenaf/glass hybrid and non-hybrid FML laminates by 12.7 mm and 20 mm hemispherical indenters	103
4.15	Load-displacement curves of kenaf/glass hybrid and non-hybrid FMLs on low velocity impact test at different energy levels	107
4.16	Load-time curves of kenaf/glass hybrid and non-hybrid FMLs from the low velocity impact test at different energy levels	111
4.17	Visible damage modes in kenaf/glass FML plates impacted at 15J with the 12.7 mm hemispherical tip	116
4.18	Visible damage modes in kenaf/glass FML plates impacted at 30J with the 12.7 mm hemispherical tip	117
4.19	Visible damage modes in kenaf/glass FML plates impacted at 45J with the 12.7 mm hemispherical tip	118
4.20	Visible damage modes in kenaf/glass FML plates impacted at 60J with the 12.7 mm hemispherical tip	119

## LIST OF APPENDICES

APPENDIX	TITLE	PAGE
A	Quasi-static indentation jig drawing	148
B	ASTM D6264	150
C	ASTM D7136	151



## LIST OF ABBREVIATIONS

AHP	- Analytical Hierarchy Process
ARALL	- Aramid Fibre Reinforced Aluminium Laminate
CARALL	- Carbon Fibre Reinforced Aluminium Laminate
CFRP	- Carbon Fibre Reinforced Polymer
CMC	- Ceramic Matrix Composites
CO <sub>2</sub>	- Carbon dioxide
ECER	- East Coast Economic Region
FML	- Fibre-Metal Laminates
FRP	- Fibre-reinforced Polymer
GLARE	- Glass Fibre Reinforced Aluminium Laminate
HDPE	- High Density Polyethylene
HVI	- High Velocity Impact
JIS	- Japanese Industrial Standard
LVI	- Low Velocity Impact
MAPP	- Maleic Anhydride Grafted Polypropylene
MMC	- Metal Matrix Composite
NaOH	- Sodium Hydroxide
OH	- Hydroxide
PLA	- Polylactic Acid

- PMC - Polymer Matrix Composite
- PP - Polypropylene
- QSI - Quasi-static indentation
- RMK - Rancangan Malaysia Ke
- ROM - Rule of Mixture
- SEM - Scanning Electron Microscopy
- SiC - Silicon Carbide
- Ti - Titanium
- UB - Unit Break
- UTM - Universal Testing Machine
- UV - Ultraviolet



## LIST OF PUBLICATIONS

Subramaniam, K., Dhar, M.S., Feng, N. and Bapokutty, O., 2017. The effects of stacking configuration on the response of tensile and quasi-static penetration to woven kenaf/glass hybrid composite metal laminate. *Polymer Composites*, 40(2), pp. 568-577.



# CHAPTER 1

## INTRODUCTION

### 1.1 Background

In line with the flourishing modern industries, demand for advanced composite structures has increased, especially for materials with better damage resistance and tolerance lead the way to produce fibre metal laminate (FML). FML refers to a class of hybrid composite structure that is based on a combination of layers of metal that sandwiched with layers of fibre-reinforced plastic, as illustrated in Figure 1.1. In 1950, the Fokker Aero structures of the Netherlands discovered that the bonded laminate structures could better prevent rapid fatigue crack growth, in comparison to monolithic materials (Chai and Manikandan, 2014).



Figure 1.1: A sample lay-up of FML

Combining composite and metal layers as bonded structures offers exceptional fatigue, impact, and damage tolerance while having the advantage of being a light-weight

material. Prior studies have reported that the fibres in the composite layers function as a barrier against crack propagation and to increase burn-through resistance, apart from providing damping and insulation, while the metal layers enhance ductility, impact resistance, and damage tolerance of the structure (Alderliesten, 2005; Cortes and Cantwell, 2006). Aramid reinforced aluminium laminate (ARALL) is the first generation of FML based on thermoset polymer matrix introduced by the Faculty of Aerospace Engineering at the Delf University of Technology in the Netherland (Villanueva and Cantwell, 2004). In the attempt to generate stronger and stiffer FMLs, several improvements were made to develop FML with varied types of synthetic fibres, such as GLARE (glass Fibre-reinforced aluminium laminate), and carbon and glass fibre forming CARALL (carbon Fibre-reinforced aluminium laminate), respectively (Sinmazçelik et al., 2011).

A comparative study on drop impact properties performed on GLARE, monolithic aluminium, and carbon Fibre-reinforced thermoplastic composite; Vlot et al. (1998) found that GLARE-FML displayed excellent damage threshold energies when compared to the two other materials. Moriniere et al. (2013) discovered that GLARE-FML displayed 86% of specific impact energy threshold, which was higher than aerospace-grade aluminium (2024-T3) in a study pertaining to impact behaviour of FML. Fan et al. (2011) investigated the thickness effect of woven glass Fibre-reinforced epoxy-based composite and FMLs on low-velocity impact by increasing the glass plies. They revealed that increment of plies in FML gave higher impact perforation resistance and energy absorbance in elastic and plastic regions.

Nonetheless, several commercial thermoset-based FMLs have been reported, such as extended polymer matrix curing time that escalates FML production cost. Hence, thermoplastic-based FMLs have been introduced with shorter fabrication time using the compression moulding technique, which eventually lowers the manufacturing cost. This

offers superior energy absorption properties and high resistance impact loading. Several studies that investigated the impact properties of thermoplastic FML (Reyes and Cantwell, 2000; Abdullah and Cantwell, 2006; Carrillo and Cantwell, 2009) support the view that thermoplastic FML structure exhibits excellent energy absorption characteristics through extensive plastic deformation in aluminium and composites layers.

The issue of recycling thermoset based FML has received considerable critical attention. Although FML production is low due to usage mainly in aerospace industry, recycling FML should be taken seriously. Yang et al. (2012) asserted that landfills might be an option for FMLs due to the higher recycling cost than manufacturing, which should be prohibited in the future. Thus, many are seeking to devise a suitable recycling method that has a less environmental impact. Mechanical separation and thermal delamination methods were investigated by Tempelman (1999) to introduce a recycling option for GLARE, since it is commercially used in the aerospace industry. GLARE scraps can be thermally delaminated and efficiently cleaned to gain back the glass fibre, but aluminium is refined back to its original quality to generate new GLARE materials for the lower-level application.

Generally, synthetic fibres have higher strength, better durability, and good corrosion and water absorption resistance properties (Khan et al., 2010a). Khan et al. (2010b) added that glass fibre is the most commercially used material as reinforcement due to its lower cost and better physico-mechanical properties than Kevlar and carbon fibres. Although wide applications of glass fibres as reinforcement for composites have successfully contributed to numerous industries, there is a rise in environmental issue at the end of their useful life. The duration for complete degradation of glass fibre takes hundreds to thousands of years due to its strong covalent bonds that connect the atoms to form excellent chemical structure. Recycling operation for synthetic Fibre-reinforced composites is economically cost-effective and eco-friendly. Nevertheless, the low economic incentive to recycle composite

material waste leads to sending it to landfills as it is relatively cheaper and as a consequence, results in landfill accumulation (Pickering, 2006).

Natural fibres have evoked the interest amongst researchers and industries for the past decades. The use of natural fibres as reinforcement material is growing due to their advantageous characteristics, such as biodegradable, acceptable strength and modulus, and cost-effective in developing materials for the engineering domain (Arthanarieswaran et al., 2014; Saba et al., 2016), unlike synthetic fibres that are hazardous to people's health and the environment. The kenaf (*hibiscus cannabinus*) fibre refers to a kind of natural fibre found abundantly in Asia. Kenaf bast fibre is lignocellulosic fibre. Generally, fibres that contain high cellulose content have high mechanical properties, wherein kenaf bast fibre and core fibre have cellulose contents as high as 60.8% and 50.6%, respectively (Ismawati, 2006; Du et al., 2008). Saba et al. (2015) highlighted that kenaf fibre could replace synthetic fibres (glass fibre) for specific mechanical applications with moderate loading condition. Nevertheless, in comparison to synthetic fibres, natural fibres are hydrophilic and possess lower modulus and strength (Alawar et al., 2009; Adekunle et al., 2011).

Recent studies have outlined the drawbacks of natural fibres that can be addressed by incorporating synthetic fibres within the same matrix to develop hybrid structures. The hybridisation of natural/synthetic fibres enhances materials' impact properties by taking the best advantages of both fibre characteristics. Natural/synthetic hybrid structures are partially degradable, recyclable, and reduce the usage of synthetic fibres. The performance of hybrid structures highly relies on several aspects: the content, the fibre, the fibre-matrix bonding, and the stacking sequence of both fibres (Jawaid and Khalil, 2011; Yahaya et al., 2014a; Saba et al., 2015). The literature vastly depicts that kenaf fibre incorporated in hybrid composites exhibits superior impact strength and displays its potential use in structural and automotive industries (Davoodi et al., 2010; Atiqah et al., 2014, Ramesh et al., 2016).