



Three-Dimensional Radiative Flow of Hybrid Nanofluid Past a Shrinking Plate with Suction

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ABSTRACT

Hybrid nanofluid has been widely used in various heat transfer applications especially as the heat exchanger due to the great thermal conductivity compared to the conventional fluid. However, numerous investigations should still be carried out to properly understand its properties. Hence, in this study, a three-dimensional radiative flow of hybrid Cu-Al₂O₃/water nanofluid past a permeable shrinking plate is numerically analyzed. The boundary layer including the energy equations are reduced to a system of ordinary differential equations using the similarity transformations and are then solved numerically by using the bvp4c solver in MATLAB. The application of suction through the permeable plate is necessary in aiding the fluid motion past the shrinking surface. Dual solutions are also observable; hence the stability analysis is conducted to mathematically validate the real solution. The enhancement of copper volumetric concentration in the hybrid nanofluid is capable in decelerating the boundary layer separation.

1. Introduction

The composition of dissimilar nanoparticles in a base fluid produces a latest generation of heat transfer fluid labelled as hybrid nanofluid. Two methods, namely the single-step method and the two-step method, are commonly applied for preparing hybrid nanofluids. According to Sidik *et al.*, [1], for small-scale formation only the single-step method is normally required, while for mass formation, the two-step method will be implemented. The application of hybrid nanofluid ranges from industrial and engineering processes (e.g., as a coolant in a heat exchanger, transformer, and nuclear system) to biomedical uses (e.g., for drug delivery in blood circulation), prompts various research to examine the rheological behaviour and the properties of heat transfer for hybrid nanofluids.

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Suresh *et al.*, [2] discussed the preparation of aqueous Cu-Al₂O₃ hybrid nanofluid, also experimentally researched the thermophysical properties and friction factor of this fluid. The friction factor and heat transfer of the studied hybrid nanofluid were greater in comparison to pure water. Then, Devi and Devi [3] developed the new thermophysical properties to study the impacts of magnetic field on Cu-Al₂O₃/water hybrid nanofluid flow at the boundary layer with the inclusion of suction over a stretching sheet. The hybrid nanofluid was contemplated to have a superior heat transfer rate in contrast to Cu/water nanofluid, and the suction parameter augments the rate of the heat transfer for both types of the fluids. Later, this study was extended by Devi and Devi [4] to a three-dimensional flow model with Newtonian heating. Meanwhile, Nadeem *et al.*, [5] discovered that the thermal slip parameter recedes the temperature of the hybrid nanofluid in a three-dimensional stagnation-point flow. The radiative effects on the three-dimensional flow of the hybrid nanofluid over a stretchable cylinder were then examined by Maskeen *et al.*, [6]. The Nusselt number, that quantifies the heat transfer rate, got enhanced by the escalation of radiation parameter. Recently, Khashi'ie *et al.*, [7] found the non-unique solutions in a problem involving the hybrid nanofluid in three-dimensional flow of past permeable and impermeable surfaces. However, only one of the solutions is stable as being revealed through the stability analysis. Other studies on Cu-Al₂O₃/water hybrid nanofluid particularly on the three-dimensional flow have been successfully accomplished by Abbas *et al.*, [8], Zainal *et al.*, [9], and Khashi'ie *et al.*, [10]. The recent interesting studies concerning on the hybrid nanofluid with variety selection of hybrid nanoparticles, parameters and methods can be found in the research papers [11–23].

Motivated by the previous research on hybrid nanofluid, the current study considers the three-dimensional boundary layer flow of hybrid Cu-Al₂O₃/water nanofluid over a permeable shrinking plate. Similarity transformations and bvp4c solver (MATLAB) are implemented to compute the solution numerically, and the results are analysed and scrutinized.

2. Model Formulation

Consider a steady, three-dimensional laminar, and incompressible hybrid nanofluid due to a permeable shrinking plate with the inclusion of thermal radiation effect and suction. The plate is deformed with a linear velocity function such that $u_w(x) = ax$ in x – direction and $v_w(y) = ay$ in y – direction where a is a constant as exhibited in Figure 1. A few of assumptions are also included for this physical model

- i. Both hybrid nanoparticles and water are in the state of thermal equilibrium.
- ii. The permeable plate assists the suction process.
- iii. Both wall and far-field temperatures are fixed and represented by T_w and T_∞ , respectively.

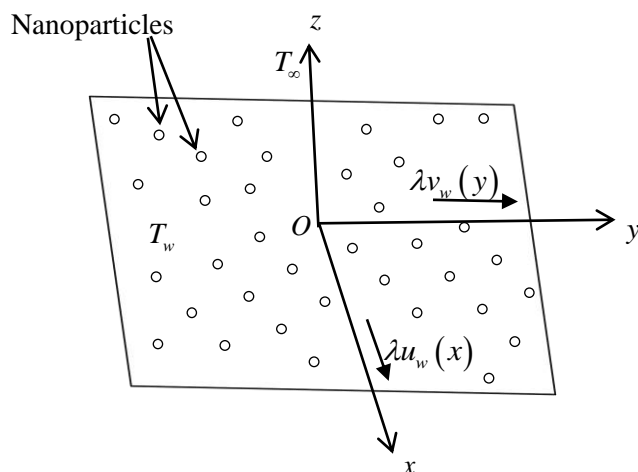


Fig. 1. The physical representation for the model

Applying and considering the boundary layer approximations as mentioned, the mathematical formulation for the model is given as [10]

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \quad (1)$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = \nu_{hmf} \frac{\partial^2 u}{\partial z^2}, \quad (2)$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = \nu_{hmf} \frac{\partial^2 v}{\partial z^2}, \quad (3)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \alpha_{hmf} \frac{\partial^2 T}{\partial z^2} - \frac{1}{(\rho C_p)_{hmf}} \frac{\partial q_r}{\partial z}, \quad (4)$$

subject to the conditions at the boundary

$$\begin{aligned} u(x, y, z) = \lambda u_w(x), \quad v(x, y, z) = \lambda v_w(y), \quad w(x, y, z) = w_0, \quad T(x, y, z) = T_w, \quad \text{at } z = 0, \\ u(x, y, z) \rightarrow 0, \quad v(x, y, z) \rightarrow 0, \quad T(x, y, z) \rightarrow T_\infty, \quad \text{as } z \rightarrow \infty. \end{aligned} \quad (5)$$

Using Rosseland [24] approximation, the heat flux term for thermal radiation in energy Eq. (4) is simplified such that

$$q_r = - \left(\frac{4\sigma^*}{3k^*} \right) \frac{\partial T^4}{\partial z}, \quad (6)$$

where σ^* and k^* are the constant of Stefan-Boltzman and the coefficient of mean absorption, accordingly. The term T^4 is expanded by using Taylor series so that $T^4 \approx 4T_\infty^3 T - 3T_\infty^4$ after neglecting the higher-order terms. Energy Eq. (4) can now exemplify by

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \left(k_{hnf} + \frac{16\sigma^* T_\infty^3}{3k^*} \right) \frac{1}{(\rho C_p)_{hnf}} \frac{\partial^2 T}{\partial z^2} \quad (7)$$

In this work, u (in x – direction), v (in y – direction) and w (in z – direction) are the velocities, T is the hybrid nanofluid temperature, $\nu_{hnf} = \mu_{hnf} / \rho_{hnf}$ and $\alpha_{hnf} = k_{hnf} / (\rho C_p)_{hnf}$ are the kinematic viscosity and the thermal diffusivity of the hybrid nanofluid, accordingly, $w_0 = -S\sqrt{av_f}$ is the mass flow that indicates the suction ($w_0 < 0$) and injection ($w_0 > 0$) for the flow.

The expression of thermophysical properties of traditional and hybrid nanofluids are presented in Table 1. For the hybrid nanofluid, the correlations by Takabi and Salehi [25] are fully adopted.

Table 1
 The expression of thermophysical properties for nanofluid

Nanofluid Properties	Hybrid	Traditional
Density	$\rho_{hnf} = \phi_1 \rho_{s1} + \phi_2 \rho_{s2} + (1 - \phi_{hnf}) \rho_f$	$\rho_{nf} = \phi \rho_s + (1 - \phi) \rho_f$
Heat Capacity	$(\rho C_p)_{hnf} = \phi_1 (\rho C_p)_{s1} + \phi_2 (\rho C_p)_{s2} + (1 - \phi_{hnf}) (\rho C_p)_f$	$(\rho C_p)_{nf} = \phi (\rho C_p)_s + (1 - \phi) (\rho C_p)_f$
Dynamic Viscosity	$\frac{\mu_{hnf}}{\mu_f} = \frac{1}{(1 - \phi_{hnf})^{2.5}}$	$\frac{\mu_{nf}}{\mu_f} = \frac{1}{(1 - \phi)^{2.5}}$
Thermal Conductivity	$\frac{k_{hnf}}{k_f} = \left[\begin{array}{l} \left(\frac{\phi_1 k_1 + \phi_2 k_2}{\phi_{hnf}} \right) + 2k_f + 2(\phi_1 k_1 + \phi_2 k_2) \\ -2\phi_{hnf} k_f \\ \left(\frac{\phi_1 k_1 + \phi_2 k_2}{\phi_{hnf}} \right) + 2k_f - (\phi_1 k_1 + \phi_2 k_2) \\ + \phi_{hnf} k_f \end{array} \right]$	$\frac{k_{nf}}{k_f} = \left[\begin{array}{l} k_s + 2k_f - 2\phi(k_f - k_s) \\ k_s + 2k_f + \phi(k_f - k_s) \end{array} \right]$

The subscripts $s1$ and $s2$ represent the nanoparticles (alumina and copper), whilst f , nf and hnf symbolize the base fluid, the nanofluid, and the hybrid nanofluid, severally. The nanoparticles volumetric concentration is denoted by ϕ_1 for alumina nanoparticle and ϕ_2 for copper nanoparticle with the hybrid nanoparticles volumetric concentration that is equated as $\phi_{hnf} = \phi_1 + \phi_2$. Also, the related thermophysical properties are displayed in Table 2, which these properties are as according to Oztop and Abu-Nada [26].

Table 2
 Thermophysical properties of nanoparticles and water

Properties	ρ (kg/m ³)	C_p (J/kgK)	k (W/mK)
Alumina	3970	765	40
Copper	8933	385	400
Water	997.1	4179	0.6130

The subsequent similarity variables (transformations) are implemented to simplify the complexity of Eq. (2), Eq. (3) and Eq. (7)

$$\eta = z \sqrt{\frac{a}{\nu_f}}, \quad u = axf'(\eta), \quad v = ayg'(\eta), \quad w = -\sqrt{av_f} [f(\eta) + g(\eta)], \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty}. \quad (8)$$

It is worth pointing out that these similarity transformations identically satisfy Eq. (1). Hence, the following ODEs are obtained:

$$\left(\frac{\mu_{mf}}{\mu_f} \right) f''' - f'^2 + (f + g) f'' = 0, \quad (9)$$

$$\left(\frac{\mu_{mf}}{\mu_f} \right) g''' - g'^2 + (f + g) g'' = 0, \quad (10)$$

$$\frac{(\rho C_p)_f}{(\rho C_p)_{mf}} \frac{1}{Pr} \left(\frac{k_{mf}}{k_f} + \frac{4}{3} Rd \right) \theta'' + (f + g) \theta' = 0, \quad (11)$$

inclusive of the boundary conditions

$$f(\eta) = S, \quad f'(\eta) = \lambda, \quad g(\eta) = 0, \quad g'(\eta) = \lambda, \quad \theta(\eta) = 1, \quad \text{at } \eta = 0, \quad (12)$$

$$f'(\eta) \rightarrow 0, \quad g'(\eta) \rightarrow 0, \quad \theta(\eta) \rightarrow 0, \quad \text{as } \eta \rightarrow \infty,$$

where S is the suction/injection parameter, $Pr = (C_p \mu)_f / k_f$ is the Prandtl number, λ is the stretching/shrinking parameter and $Rd = 4\sigma^* T_\infty^3 / k_f k^*$ is the thermal radiation parameter.

The skin friction coefficients C_{fx} (in x – direction) and C_{fy} (in y – direction) as well as the local Nusselt number Nu_x , are respectively specified by [10]

$$C_{fx} = \frac{\tau_{wx}}{\rho_f u_w^2}, \quad C_{fy} = \frac{\tau_{wy}}{\rho_f v_w^2}, \quad Nu_x = \frac{xq_w}{k_f (T_w - T_\infty)}, \quad (13)$$

where the surface shear stresses and the surface heat flux, are specified as

$$\tau_{wx} = \mu_{mf} \left(\frac{\partial u}{\partial z} \right)_{z=0}, \quad \tau_{wy} = \mu_{mf} \left(\frac{\partial v}{\partial z} \right)_{z=0}, \quad q_w = -k_{mf} \left(\frac{\partial T}{\partial z} \right)_{z=0} + (q_r)_{z=0}. \quad (14)$$

Substituting Eq. (8) and Eq. (14) into Eq. (13), C_{fx} , C_{fy} and Nu_x can be simplified as

$$C_{fx} \text{Re}_x^{1/2} = \frac{\mu_{mf}}{\mu_f} f''(0), \quad C_{fy} \text{Re}_y^{1/2} = \frac{\mu_{mf}}{\mu_f} g''(0), \quad Nu_x \text{Re}_x^{-1/2} = - \left(\frac{k_{mf}}{k_f} + \frac{4}{3} Rd \right) \theta'(0), \quad (15)$$

respectively, where $Re_x = xu_w / \nu_f$ and $Re_y = yv_w / \nu_f$.

Eq. (9)-(11) together with the boundary conditions (12) are solved numerically by using the *bvp4c* solver in MATLAB with the appropriate values of parameter to compute the profiles and the main physical quantities. Further explanation on the numerical computation in the *bvp4c* solver can be seen in the published paper elucidated by Khashi'ie *et al.*, [10].

3. Stability Analysis

The stability analysis execution requires a few steps, which firstly, as recommended by Merkin [27], Eq. (2), Eq. (3) and Eq. (7) need to be transformed into the unsteady state

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \frac{\partial u}{\partial t} = \nu_{hmf} \frac{\partial^2 u}{\partial z^2}, \tag{16}$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \frac{\partial v}{\partial t} = \nu_{hmf} \frac{\partial^2 v}{\partial z^2}, \tag{17}$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} + \frac{\partial T}{\partial t} = \left(k_{hmf} + \frac{16\sigma^* T_\infty^3}{3k^*} \right) \frac{1}{(\rho C_p)_{hmf}} \frac{\partial^2 T}{\partial z^2}, \tag{18}$$

and a new set of similarity transformations including the dimensionless time variable τ are introduced,

$$\eta = z \sqrt{\frac{a}{\nu_f}}, \quad \tau = at, \quad \theta(\eta, \tau) = \frac{T - T_\infty}{T_w - T_\infty}, \tag{19}$$

$$u = ax \frac{\partial f(\eta, \tau)}{\partial \eta}, \quad v = ay \frac{\partial g(\eta, \tau)}{\partial \eta}, \quad w = -\sqrt{a\nu_f} [f(\eta, \tau) + g(\eta, \tau)].$$

By applying the transformations (19) into Eq. (16)-(18), the equations are then transformed to:

$$\left(\frac{\mu_{hmf}}{\rho_{hmf}} \frac{\partial^3 f}{\partial \eta^3} - \left(\frac{\partial f}{\partial \eta} \right)^2 \right) + (f + g) \frac{\partial^2 f}{\partial \eta^2} - \frac{\partial^2 f}{\partial \eta \partial \tau} = 0, \tag{20}$$

$$\left(\frac{\mu_{hmf}}{\rho_{hmf}} \frac{\partial^3 g}{\partial \eta^3} - \left(\frac{\partial g}{\partial \eta} \right)^2 \right) + (f + g) \frac{\partial^2 g}{\partial \eta^2} - \frac{\partial^2 g}{\partial \eta \partial \tau} = 0, \tag{21}$$

$$\frac{(\rho C_p)_f}{(\rho C_p)_{hmf}} \frac{1}{Pr} \left(\frac{k_{hmf}}{k_f} + \frac{4}{3} Rd \right) \frac{\partial^2 \theta}{\partial \eta^2} + (f + g) \frac{\partial \theta}{\partial \eta} - \frac{\partial \theta}{\partial \tau} = 0, \tag{22}$$

conditioned to

$$f(\eta, \tau) = S, \quad g(\eta, \tau) = 0, \quad \frac{\partial f(\eta, \tau)}{\partial \eta} = \lambda, \quad \frac{\partial g(\eta, \tau)}{\partial \eta} = \lambda, \quad \theta(\eta, \tau) = 1, \quad \text{at } \eta = 0, \quad (23)$$

$$\frac{\partial f(\eta, \tau)}{\partial \eta} \rightarrow 0, \quad \frac{\partial g(\eta, \tau)}{\partial \eta} \rightarrow 0, \quad \theta(\eta, \tau) \rightarrow 0, \quad \text{as } \eta \rightarrow \infty.$$

Then, the perturbation equations are adopted to test the solutions' stability which are equated as [10,25]

$$\left. \begin{aligned} f(\eta, \tau) &= f_0(\eta) + e^{-\gamma\tau} F(\eta), \quad f(\eta) = f_0(\eta) \\ g(\eta, \tau) &= g_0(\eta) + e^{-\gamma\tau} G(\eta), \quad g(\eta) = g_0(\eta) \\ \theta(\eta, \tau) &= \theta_0(\eta) + e^{-\gamma\tau} H(\eta), \quad \theta(\eta) = \theta_0(\eta) \end{aligned} \right\} \quad (24)$$

where $F(\eta)$, $G(\eta)$ and $H(\eta)$ are the small relative to $f_0(\eta)$, $g_0(\eta)$ and $\theta_0(\eta)$, respectively, and γ is the yet undetermined eigenvalue. Therefore, by employing Eq. (24) into Eq. (20)-(22), the linearized eigenvalue problem can be formulated as

$$\left(\frac{\mu_{mf} / \mu_f}{\rho_{mf} / \rho_f} \right) F''' + (f_0 + g_0) F'' + (F + G) f_0'' - (2f_0' - \gamma) F' = 0, \quad (25)$$

$$\left(\frac{\mu_{mf} / \mu_f}{\rho_{mf} / \rho_f} \right) G''' + (f_0 + g_0) G'' + (F + G) g_0'' - (2g_0' - \gamma) G' = 0, \quad (26)$$

$$\frac{(\rho C_p)_f}{(\rho C_p)_{mf}} \frac{1}{Pr} \left(\frac{k_{mf}}{k_f} + \frac{4}{3} Rd \right) H'' + (F + G) \theta_0' + (f_0 + g_0) H' + \gamma H = 0, \quad (27)$$

and following the relaxation boundary conditions as recommended by Harris *et al.*, [28], ($F'(\eta) \rightarrow 0$ is initially relaxed and reinstated with $F''(0) = 1$) the boundary conditions are stated as

$$F(\eta) = 0, \quad G(\eta) = 0, \quad H(\eta) = 0, \quad F'(\eta) = 0, \quad G'(\eta) = 0, \quad F''(\eta) = 1, \quad \text{at } \eta = 0, \quad (28)$$

$$G'(\eta) \rightarrow 0, \quad H(\eta) \rightarrow 0, \quad \text{as } \eta \rightarrow \infty.$$

The linearized eigenvalue problem (25)-(27) with (28) will be solved by the utilization of bvp4c solver to execute the eigenvalue γ . The smallest eigenvalue γ will reveal the stability of the solutions, in which the smallest positive eigenvalue ($\gamma > 0$) deduces that the flow/solution is stable/real due to the initial decay of disturbance and otherwise. Additionally, instead of analysing on the sign (positive/negative) of the smallest eigenvalue, the stability of the solution can also be recognized by looking at the graphical representation of the solution towards the velocity and temperature profiles, the skin friction coefficient and the local Nusselt number. Normally, when there are dual solutions, the solution that is closer to the boundary or has the least boundary layer thickness is considered as the stable solution compared to the other one. Also, by looking through the graph of the skin friction coefficient and the local Nusselt number, the upper branch of the solution is said to be stable than the lower branch when there exist dual solutions. However, it is

necessary to analyse the stability of the solution through the execution of the eigenvalues for a sophisticated validation.

4. Results and Discussions

The effects of volumetric concentration of copper ϕ_2 , thermal radiation Rd , suction S , and stretching/shrinking surface λ parameters are scrutinized in the model of boundary layer flow (three dimensional) of Cu-Al₂O₃/water hybrid nanofluid over a permeable shrinking plate. The mathematical formulation that governs such boundary layer flow model is solved and the numerical solutions are enumerated, assisted by bvp4c solver that is accessible in MATLAB. Certain related values for the boundary layer thickness, initial guesses and parameters are adjusted accordingly to ensure the accuracy of the solutions. For validation purposes, a comparison analysis has been performed for $-f''(0)$ and $-g''(0)$ obtained in this present study with the previous related models as tabulated in Table 3. The compared values are noticed to be well agreed, hence validate the numerical solutions together with the taken numerical procedure.

Table 3

$-f''(0)$ and $-g''(0)$ when $S = \phi_1 = \phi_2 = Rd = 0$ and $\lambda = 1$ (stretching case)

	$-f''(0)$	$-g''(0)$
Present (bvp4c)	1.173721	1.173721
Khashi'ie <i>et al.</i> , [10] (bvp4c)	1.173721	1.173721
Jusoh <i>et al.</i> , [29] (bvp4c)	1.173721	1.173721
Hayat <i>et al.</i> , [30] (HAM)	1.173721	1.173721

In this study, we have fixed the value for Prandtl number, $Pr = 6.2$ and the volumetric concentration for alumina, $\phi_1 = 0.01$ thoroughly, while the other parameters are set to be varied with the appropriate range of values. Dual solutions are observable specifically when the surface is shrunk ($\lambda < 0$) with appropriate value of suction parameter S . The impact of volumetric concentration parameter ϕ_2 for copper towards the skin friction coefficients $Re_x^{1/2} C_{fx}$, $Re_y^{1/2} C_{fy}$ against shrinking surface ($\lambda < 0$) and suction S parameters are illustrated in Figure 2 and Figure 3. The intensification of copper volumetric concentration parameter ϕ_2 has intensified the skin friction coefficients $Re_x^{1/2} C_{fx}$, $Re_y^{1/2} C_{fy}$ at the shrinking surface ($\lambda < 0$) for the first solution. In Figure 2, the critical points which located in between the first and the second solutions are visible in the shrinking surface region, apparently at $\lambda_{c1} = -1.8772$ ($\phi_2 = 0.01$), $\lambda_{c2} = -1.9199$ ($\phi_2 = 0.015$) and $\lambda_{c3} = -1.9610$ ($\phi_2 = 0.02$) with the condition of $S = 3.5$ and $Rd = 2$. Meanwhile, in Figure 3, the critical point is located at $S_{c1} = 2.5545$ ($\phi_2 = 0.01$), $S_{c2} = 2.5260$ ($\phi_2 = 0.015$) and $S_{c3} = 2.4994$ ($\phi_2 = 0.02$) when $\lambda = -1$ and $Rd = 2$. These critical points also indicate the occurrence point for boundary layer separation, by cause of the enhancement of copper volumetric concentration parameter ϕ_2 .

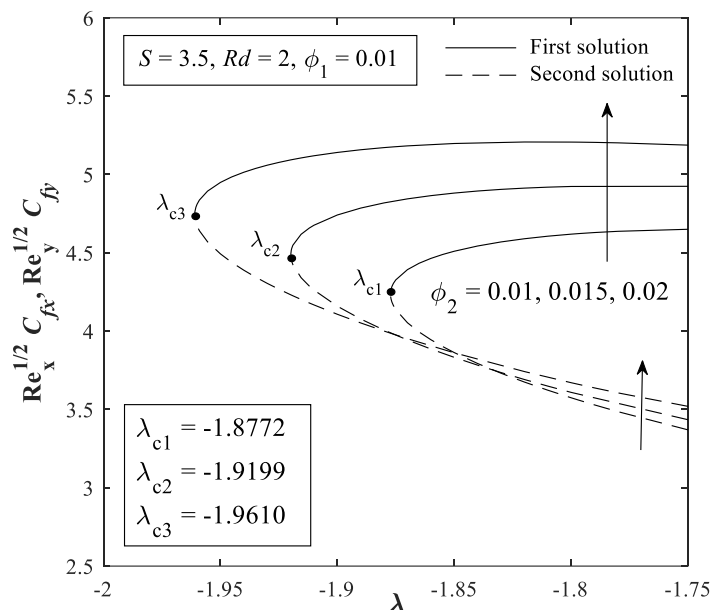


Fig. 2. The skin friction coefficients with λ for diverse ϕ_2

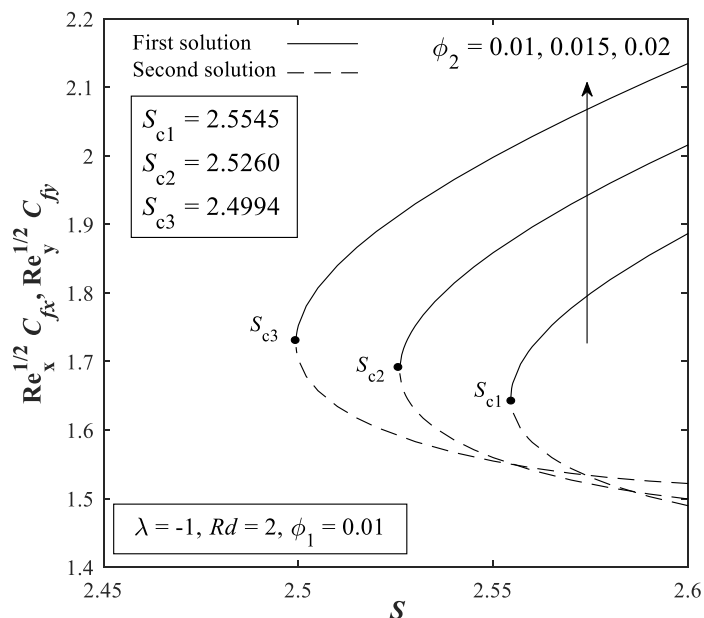


Fig. 3. The skin friction coefficients with S for diverse ϕ_2

The effects of copper volumetric concentration ϕ_2 and thermal radiation Rd parameters towards the heat transfer rate which is measured by the local Nusselt number $Re_x^{-1/2} Nu_x$ are depicted in Figure 4 to Figure 7 against the shrinking surface ($\lambda < 0$) and suction S parameters, accordingly. In these figures, the local Nusselt number $Re_x^{-1/2} Nu_x$ is noticed to gradually reduced when the shrinking surface ($\lambda < 0$) and suction S parameters decrease. Figure 4 and Figure 5 show that the local Nusselt number $Re_x^{-1/2} Nu_x$ is affected to be reduced when the copper volumetric concentration parameter ϕ_2 is enhanced in the shrinking surface region ($\lambda < 0$) for both of the solutions. The critical points are observable at the shrinking surface region ($\lambda < 0$) as well, located similarly as mentioned in Figure 2 and Figure 3 but with a different condition of thermal radiation parameter Rd which is set to be $Rd = 0.02$. This also could deduce that the thermal radiation parameter Rd does not affect

the boundary layer separation point. Consequently, in Figure 6 and Figure 7, it is also noticeable that the different values of thermal radiation parameter Rd only approach towards the same critical point which is located at $\lambda_c = -1.8772$ and $S_c = 2.5545$ for $Rd = 0, 0.01, 0.02$ against the shrinking surface ($\lambda < 0$) and suction S parameters, respectively. Nevertheless, the intensification of thermal radiation parameter Rd leads to the enhancement of the local Nusselt number $Re_x^{-1/2} Nu_x$. In addition, it is also worth mentioning that the revelation of the critical point is important as it can signify the separation point of the boundary layer which is the point where the occurrence of the transition of the flow is changed from laminar to turbulent. Hence, to delay such occurrence, an appropriate adjustment on the parameter related to the critical point can be done to delay the separation process and to ensure the stability of the flow.

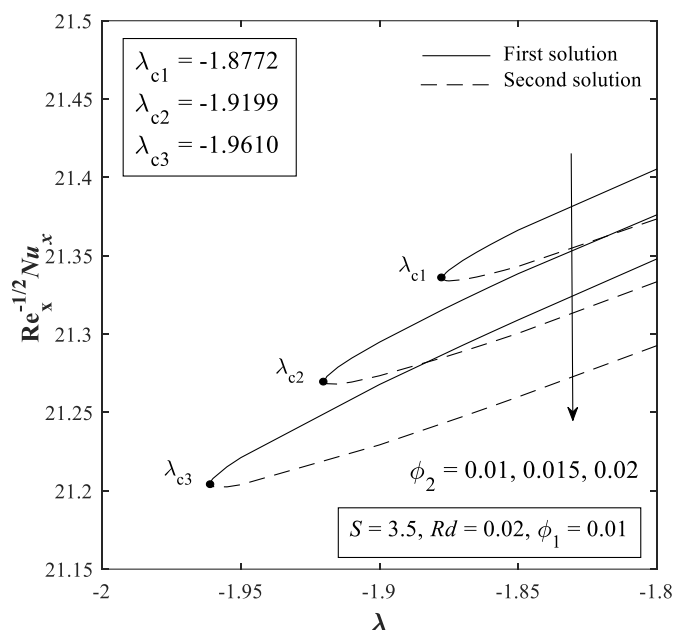


Fig. 4. The local Nusselt number with λ for diverse ϕ_2

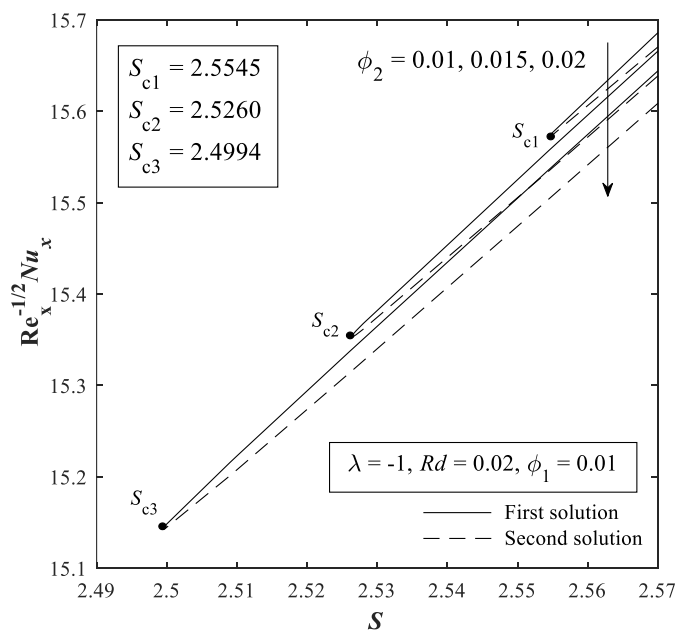


Fig. 5. The local Nusselt number with S for diverse ϕ_2

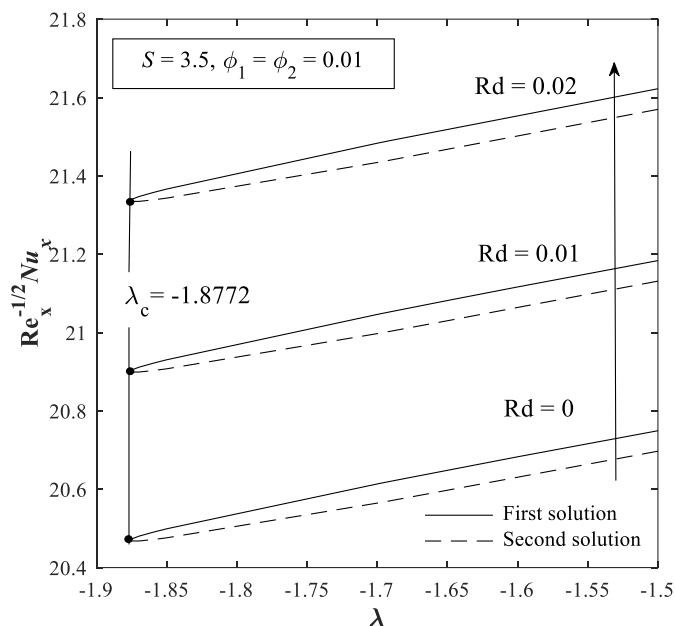


Fig. 6. The local Nusselt number with λ for diverse Rd

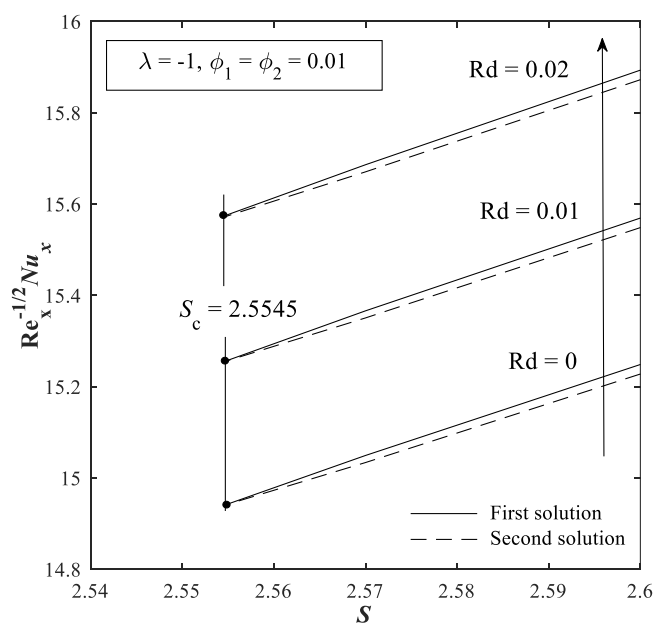


Fig. 7. The local Nusselt number with S for diverse Rd

The velocity profiles $f'(\eta)$, $g'(\eta)$ and temperature profile $\theta(\eta)$ for diverse values of copper volumetric concentration ϕ_2 , suction S and thermal radiation Rd parameters at the shrinking surface ($\lambda < 0$) are exhibited in Figure 8 to Figure 12. The profiles also are seen to meet the far-field boundary layer condition. Figure 8 and Figure 9 reveals that the enhancement of copper volumetric concentration ϕ_2 and suction S parameters have caused the velocity profiles $f'(\eta)$, $g'(\eta)$ for the first solution to accelerate and decelerate for the second solution. Meanwhile, for the temperature profile $\theta(\eta)$, as noticeable in Figure 10, the intensification of copper volumetric concentration ϕ_2 has intensified the temperature profile $\theta(\eta)$ and thickening the boundary layer thicknesses for the first and second solutions. Unlikely, for the suction S and thermal radiation Rd parameters, the

intensification in these parameters causes the temperature profile $\theta(\eta)$ and the boundary layer thicknesses to be reduced for both solutions. In this specified case, both suction and thermal radiation parameters could act as a coolant agent.

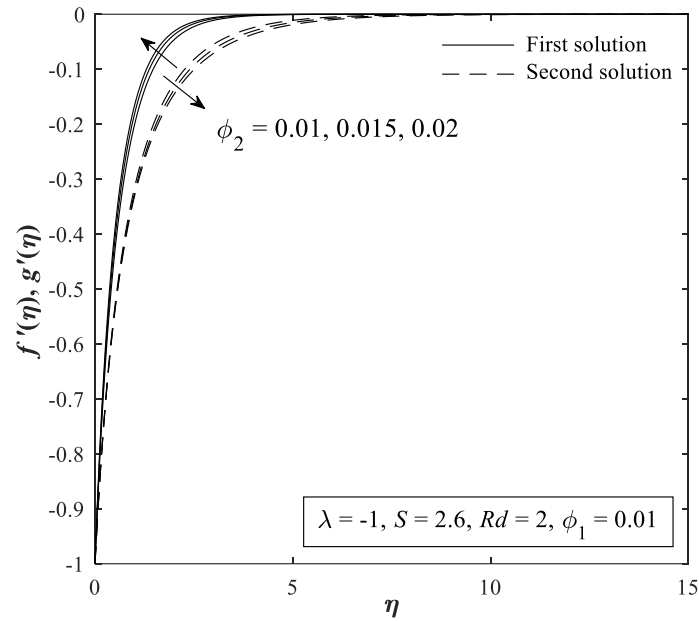


Fig. 8. Velocity profiles for diverse ϕ_2

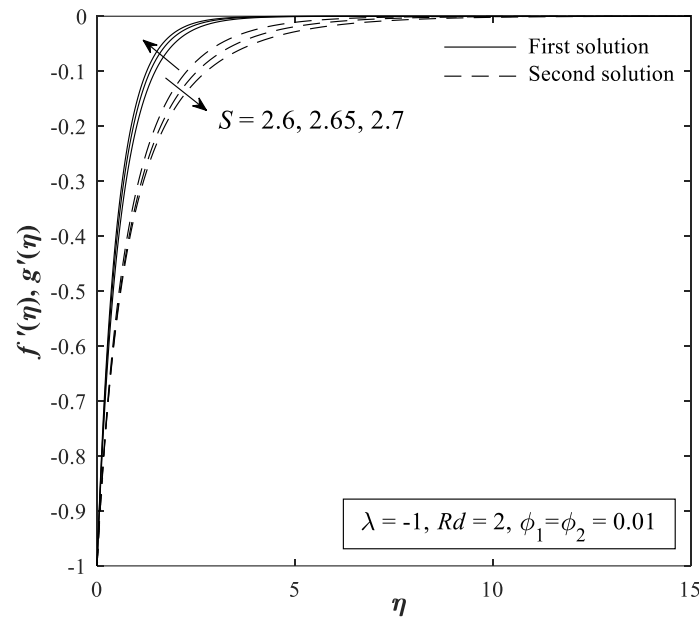


Fig. 9. Velocity profiles for diverse S

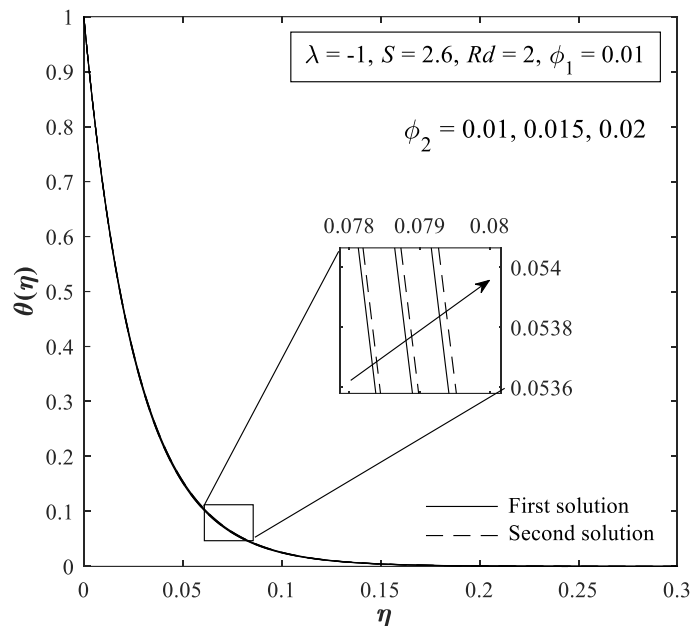


Fig. 10. Temperature profile for diverse ϕ_2

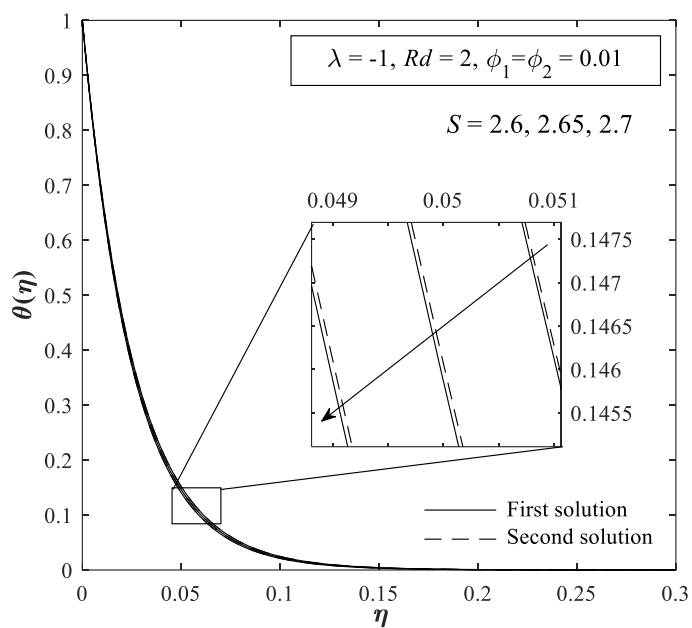


Fig. 11. Temperature profile for diverse S

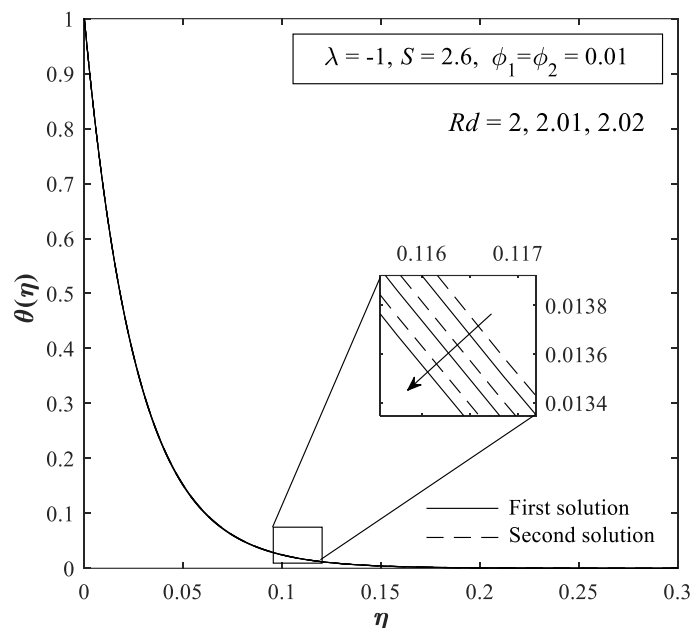


Fig. 12. Temperature profile for diverse Rd

In this study, the stability analysis is executed in consequence to the existence of dual solutions, as to discover which solution is stable among the dual solutions. The formulation for the analysis is performed as shown in Section 3 with the aid of bvp4c solver. Figure 13 graphically presents the smallest eigenvalues γ against the stretching/shrinking surface parameter λ when $S = 3.5$, $Rd = 2$ and $\phi_2 = 0.01$ with the selected critical point of $\lambda_c = -1.8772$. The first solution is noticed to have the positive smallest eigenvalues, whereas the second solution produces the negative smallest eigenvalues. This implies that the first solution is real/stable, and adversely for the other one. It is also notable that, $\gamma \rightarrow 0$ as $\lambda \rightarrow \lambda_c$.

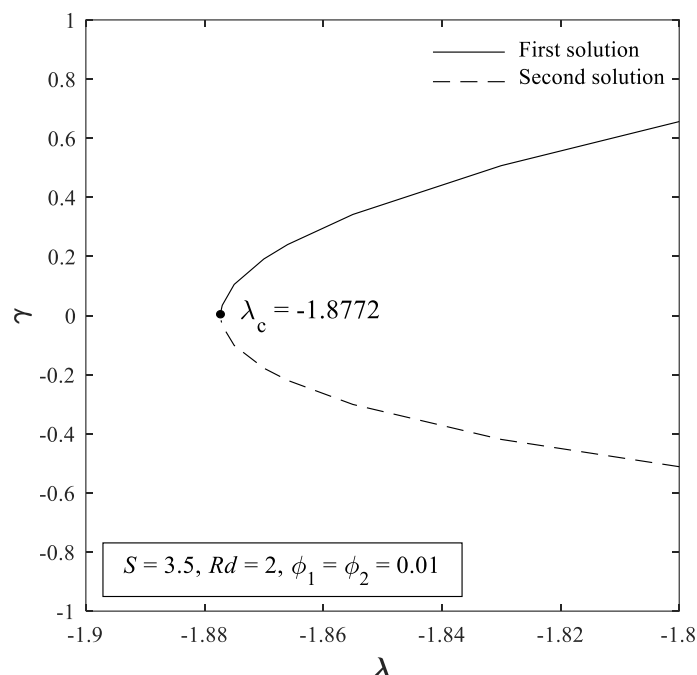


Fig. 13. The smallest eigenvalue γ with λ

5. Conclusion

The three-dimensional flow of boundary layer for hybrid Cu-Al₂O₃/water nanofluid on a permeable shrinking plate is modeled and solved in this study. The numerical solution is computed, and the stability analysis is conducted with the used bvp4c solver (MATLAB). The results can be summarized as follows

- i. Dual solutions are notable to exist, and only the first solution is real and stable.
- ii. The intensification of copper volumetric concentration decelerated the boundary layer separation.
- iii. The boundary layer separation is unimpacted by the thermal radiation parameter.
- iv. The skin friction coefficients can be enhanced with the intensification of copper volumetric concentration.
- v. The heat transfer rate is augmented with the intensification of thermal radiation parameter and is reduced with the intensification of copper volumetric concentration parameter.
- vi. The reduction of stretching/shrinking surface and suction parameters leads the local Nusselt number to reduce.
- vii. The velocity profiles for the first solution are enhanced with the incrementation of copper volumetric concentration and suction parameters.
- viii. The temperature profile is intensified with the incrementation of copper volumetric concentration parameter but is reduced with the incrementation of suction and thermal radiation parameters.

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